

SUNVALE HOMES

FUNCTIONAL SERVICING REPORT

DEY DRIVE TOWNHOUSES
TOWN OF COLLINGWOOD

JUNE 2026

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1. INTRODUCTION

Cobide Engineering Inc. was retained by Sunvale Homes to provide engineering services in support of a Draft Plan of Subdivision Approval Application. The application will be to develop the property into a 33-unit street townhouse development.

A copy of the proposed Site Plan has been included in Appendix A as Drawing SP1.

1.1 LOCATION

The proposed development is located on Block 183, Registered Plan 51M-945, Geographic Township of Nottawasaga, Town of Collingwood, County of Simcoe (described herein as the “site”). A Site Location Map is included as Figure 1. The subject property is approximately 1.918 hectares in area.

1.2 DEVELOPMENT PROPOSAL

The proposed development consists of 1.918 hectares of land within the Collingwood settlement area.

The proposed plan is to develop the site into a residential subdivision. The subdivision will involve the extension of Dey Drive from Kirby Avenue.

A single road access point to Kirby Avenue will be provided. There will be a number of pedestrian linkages to the nearby trail network.

The proposed development is within the Collingwood Settlement Boundary of the current Official Plan and thus is intended for servicing from municipal water and sewage systems.



MAP SOURCE - MTO ROAD MAP



COBIDE
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Client/Project

PROPOSED TOWNHOUSE DEVELOPMENT
TOWN OF COLLINGWOOD
DEY DRIVE TOWNHOUSES
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Figure No.

1

Title

REGIONAL LOCATION MAP

2. WATER DISTRIBUTION SYSTEM

The water distribution system will be sized based on the existing conditions at the connection to the municipal system and the subdivisions demands which are determined by the Ministry of the Environment (MOE) Design Guidelines for Drinking-Water Systems (2008).

2.1 DESIGN CRITERIA

The water distribution system will be design in accordance MOE guidelines which state the system “should be designed to satisfy the greater of the following demands:

- *Maximum day demand plus fire flow; or,*
- *Peak hour demand*

The maximum day demand and peak hour demand are based on the projected water consumption from the development and the fire flow is based on the type of the development.

The system will require modelling during the detailed design stage to ensure the water pressure throughout the system is within the requirements of the MOE.

Based on MOE guidelines, the minimum pressure at ground level at all points in the distribution system under maximum day demand plus fire flow conditions are to be 140 kPa (20 psi). The normal operation pressure should be between 350 kPa (50 psi) to 480 kPa (70 psi). There shall be no point in the distribution system that has a normal operating pressure of less than 275 kPa (40 psi). The maximum pressure in the pipe cannot exceed 700 kPa (100 psi).

2.2 WATER CONSUMPTION

The system will be designed based on a domestic water demand of 260 L/cap/day as per the Town of Collingwood Development Standards. The peaking factors will be derived from the Town of Collingwood Development Standards. The peaking factor for the maximum day demand will be 1.77 and the peaking factor for the peak hour demand will be 2.7. This population estimate is based on 2.4 people per townhouse as per the Town of Collingwood Development Standards.

Table 1 below summarizes the projected maximum day and peak hour demands for the proposed development.

Table 1 - Proposed Water Demands

Demand	Population	Consumption (L/cap/day)	Peaking Factor	Peak Rate (L/day)	Peak Rate (L/s)
Maximum Day	80	260	1.77	36,816	0.43
Peak Hour	80	260	2.7	56,160	0.65

2.3 FIRE FLOW

The AWWA *Manual of Water Supply Practices M31 – Distribution System Requirements for Fire Protection* and the Fire Underwriters Survey document *Water Supply for Public Fire Protection* will determine the required fire flows.

The fire flows are dependent upon many factors including the type of construction materials, building height and density of the development.

The fire flow requirements for a typical townhouse within the development are expected to 8000 L/min which would need to be sustained for 1.5 hours.

2.4 DESIGN FLOW RATES

The watermain within the subdivision will be required to maintain the aforementioned pressure while supplying 133.8 L/s (MDD + Fire Flow). The pipes should be designed with a pipe roughness C-value of 110 which is typically used to represent PVC pipe.

2.5 WATERMAIN CONFIGURATION

The proposed watermain will be connected to the municipal system at the proposed intersection with Kirby Avenue. There is currently a 200mm diameter Ductile Iron watermain on the south side of Kirby Avenue. This watermain will provide service to the proposed development. It is proposed to connect to the main at the Dey Drive and Kirby Avenue intersection. An easement has been negotiated with the adjacent developer for storm sewer servicing.

A 200mm diameter Ductile Iron watermain is proposed within the development. There will be no irrigation systems within the development.

A single connection will be provided to each residential lot using 19mm diameter copper water services. Each unit will be individually metered.

2.6 AVERAGE DAY DEMAND (ICBL)

As per the Town's ICBL, Public Works has identified water servicing based on a standard unit of measure as an SDU (Single Detached Unit). A Townhouse unit is equivalent to 0.83 SDU's. Therefore, this development will require **27.4 SDU's** of water and wastewater capacity.

3. SANITARY SEWER SYSTEM

The sanitary sewer system will be sized based on the existing conditions at the connection to the municipal system and the subdivisions demands which are determined by the Ministry of the Environment (MOE) Design Guidelines for Sewage Works (2008).

3.1 DESIGN CRITERIA

The sanitary sewer system will be design in accordance MOE guidelines.

The sanitary sewer will be designed to convey the projected peak flow based upon the projected population of the development, flows from future development to the north as well as extraneous flows.

3.2 DESIGN FLOW RATES

The sanitary sewer will be designed based on a peak flow of 260 L/cap/day and a peaking factor of 4.0 for the size of the development. Based on a population of 80 the projected residential flow is 0.96 L/s. The development will contribute 1.918 ha of extraneous flows to the sanitary sewer. This will contribute 0.44 L/s to the flow. Therefore, the peak flow from the development is 1.40 L/s.

The average daily domestic sanitary sewer flows will be designed based on a peak flow of 260 L/cap/day as per the latest Town of Collingwood Development Standards. Based on a population of 80 the projected residential flow is 20,800 L/day. The development will contribute 1.918 ha of extraneous flows to the sanitary sewer. This will contribute 38,114 L/day to the flow. Therefore, the average daily flow from the development is expected to be 58,914 L/day as per the Town of Collingwood's latest Development Standards.

3.3 SANITARY SEWER CONFIGURATION

There will be a sanitary sewer on the proposed streets with a single connection to the existing sanitary sewer at Dey Drive and Kirby Avenue. A single connection will be provided to each residential lot.

All sanitary sewers are proposed to be 200mm diameter PVC pipe. The minimum slope considered will be 0.40% to maintain a minimum velocity at full flow to prevent sediment deposition and blockages. The furthest section upstream will be installed at 1.0% for that same reason where possible.

4. STORM SEWER SYSTEM

The storm sewer system will be design in accordance with the municipal and conservation authority guidelines including the Ministry of the Environment (MOE) Design Guidelines. The storm sewer system will use the rationale method to size the storm sewer to accommodate the 100 year peak flow from the development. This will ensure that all runoff from the development reaches the SWM Pond. The runoff from the back of the proposed lots will drain towards the storm water system along grass swales and ditch inlet catchbasins.

The existing pond north of Kirby Avenue will be used to provide quality and quantity control. The use of the existing pond and the easement required has been worked out between the two developers.

The previously completed Pretty River Floodplain Analysis determined the regulatory floodplain in the area of this development required that the lowest opening of all dwelling units would need to be at a minimum elevation of 194.50m. The Tatham response to NVCA has been included in Appendix D outlining this requirement. The grading of the site has ensured that the lowest grade at the buildings is at minimum 194.80m.

As per the SWM report from the Eden Oak development, there is approximately 800 m³ extra quality control volume which will adequately treat the runoff from the proposed development. The development will require 76 m³. The existing development and the proposed development have been modelled using PCSWMM to ensure the existing pond can control the additional flows. As shown in Table 2, below during both the SCS and Chicago design storm events there is very little increase in peak flows. The combined outflows are still significantly lower than pre-development conditions.

Table 2 – Stormwater Flows

Storm Event	Pre Development Flow (m³/s)	Eden Oak Only Flow (m³/s)	Combined Post Development Flow (m³/s)
SCS 2 Year	0.148	0.024	0.029
SCS 5 Year	0.208	0.027	0.033
SCS 25 Year	0.485	0.035	0.040
SCS 100 Year	0.641	0.039	0.059
Chicago 2 Year	0.121	0.023	0.028
Chicago 5 Year	0.226	0.027	0.031
Chicago 25 Year	0.426	0.032	0.037
Chicago 50 Year	0.524	0.034	0.039
Chicago 100 Year	0.624	0.036	0.041

As seen in the table above, the combined post development peak flows remain considerably lower than pre-development peak flows.

5. GRADING & EROSION AND SEDIMENT CONTROL

Erosion and sediment controls shall meet the requirements of the most recent version of the MOE *Stormwater Management Planning and Design Manual* at the time of construction.

5.1 CONSTRUCTION STAGE

Prior to the start of construction, appropriate sediment control facilities are to be in place. Following are details regarding erosion and sediment control that are to be implemented:

- Placement of heavy duty siltation fencing is required along the east, west and south sides of the site to intercept sediment that could potentially be transported by sheet flow across the site.
- Placement of temporary straw check dams within swales and any other locations where a concentrated flow of runoff may occur. All proposed drainage swales are to be seeded during construction;
- Installation of filter cloth under all new and existing catchbasin grates until paving of the subdivision streets is completed;
- Mud mats will be placed at construction accesses to keep public roadways free from debris during the construction period.
- Re-vegetate all disturbed areas after underground and surface works have been constructed.

Prior to removal of sediment control facilities, ensure that sediment that may have accumulated has been removed. Once the area has been stabilized, the silt fencing can be removed.

5.2 LOT DEVELOPMENT

During individual construction of units within the development, silt barriers are to be constructed, as appropriate, to prevent the eroding of materials into the roadside drainage system. The sedimentation control can be in the form of siltation fences placed in the direction of flow from the construction site and shallow excavated sediment traps (moats) should be constructed around any stockpiled materials.

The responsibility for the individual lot sediment control is the landowner/builder constructing the dwelling.

The proposed grading design will match all existing grades at the property lines and will not alter or affect the drainage patterns of the neighbouring properties. The proposed site grading will drain the stormwater through side yard swales and a storm sewer system. The majority of the slopes found on site are proposed to be between 2.0% and 6.0%.

Sincerely,

Cobide Engineering Inc.



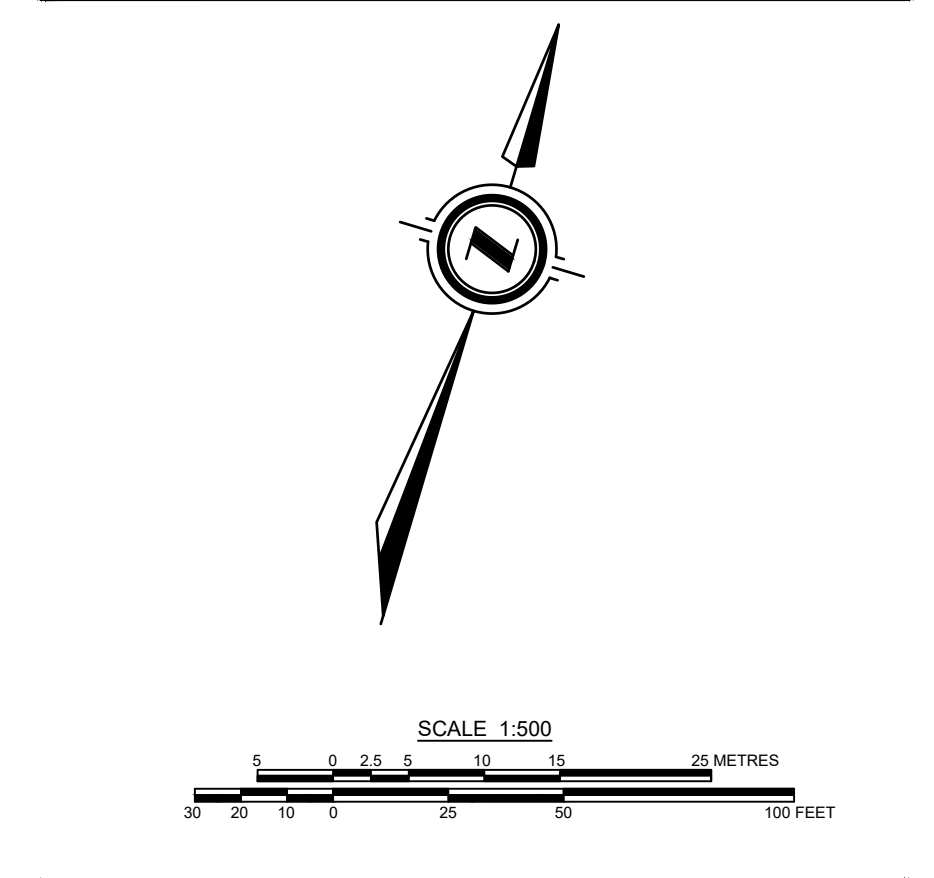
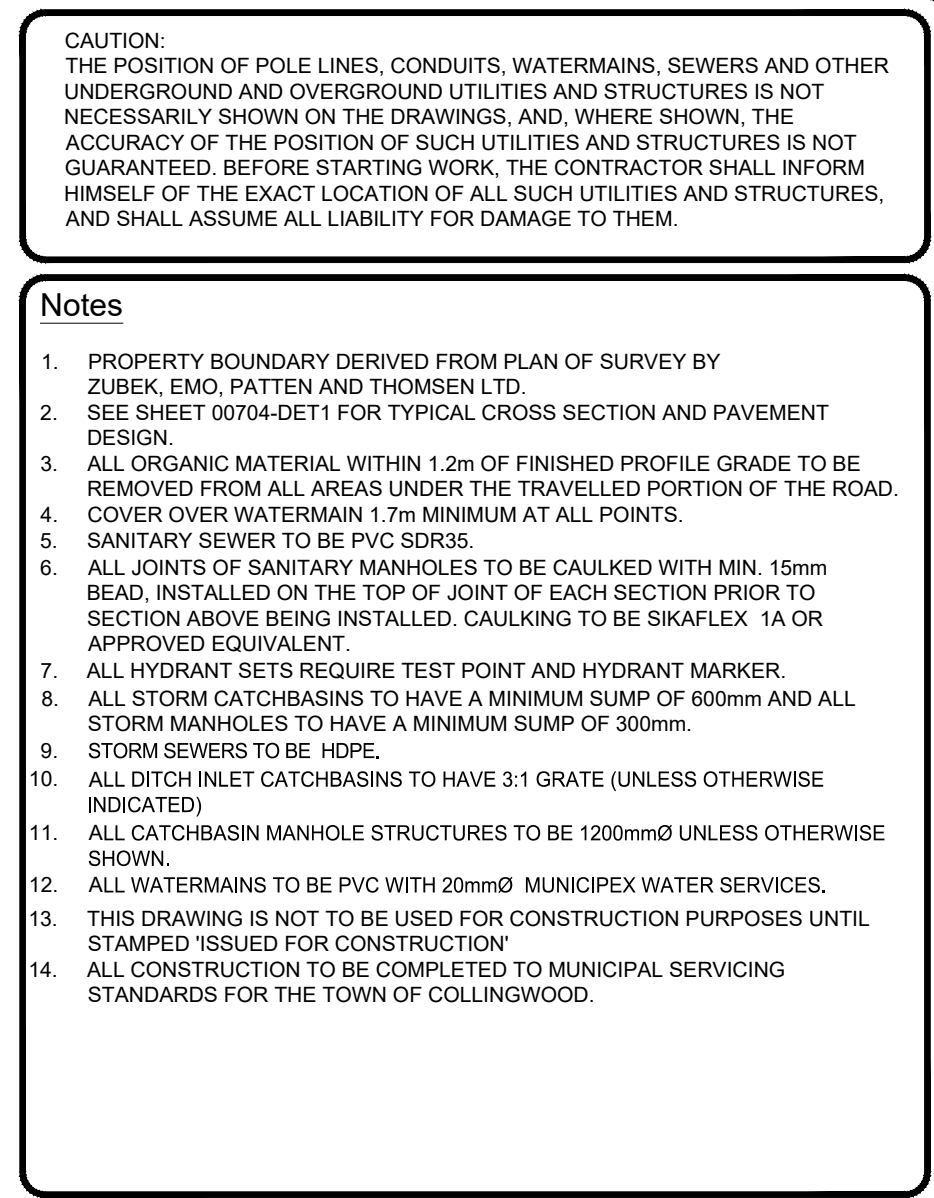
Travis Burnside, P. Eng.

Appendix A

DRAWINGS

FUNCTIONAL SERVICING REPORT

**DEY DRIVE TOWNHOUSES
TOWN OF COLLINGWOOD**



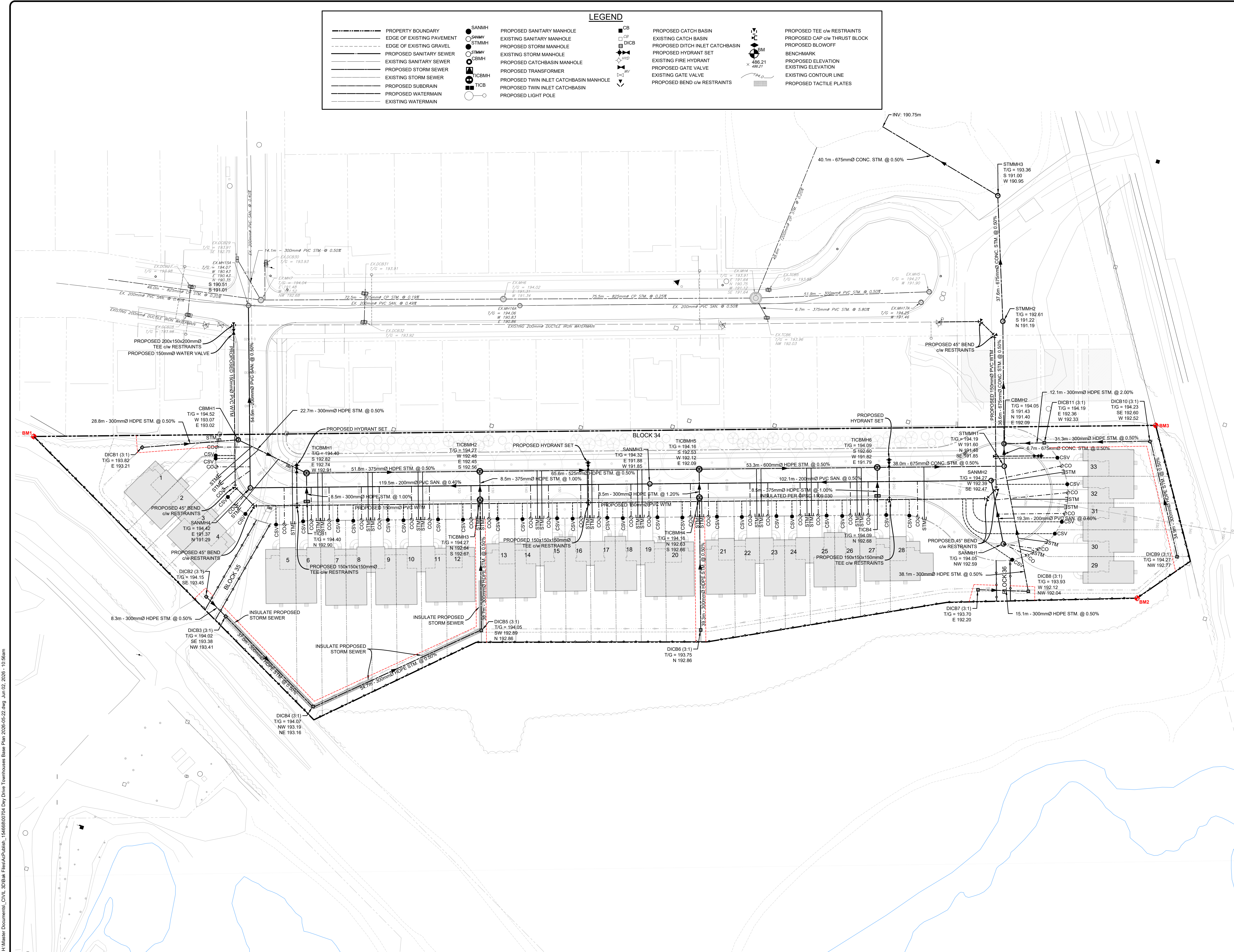
<u>Benchmark Information</u>		
 BM1	TOP OF STANDARD IRON BAR LOCATED AT THE WESTERLY CORNER OF THE PROPERTY (AS SHOWN ON DRAWINGS)	194.413m
	ELEVATION	
 BM2	TOP OF STANDARD IRON BAR LOCATED AT THE SOUTH-EASTERLY CORNER OF THE PROPERTY (AS SHOWN ON DRAWINGS)	194.002m
	ELEVATION	
 BM3	TOP OF STANDARD IRON BAR LOCATED AT THE NORTHERLY CORNER OF THE PROPERTY (AS SHOWN ON DRAWINGS)	192.851m
	ELEVATION	

4	JUN 02/26	THIRD SUBMISSION	TLB	SJC	
3	APR 08/26	SECOND SUBMISSION	TLB	SJC	
2	DEC 08/25	REVISED FIRST SUBMISSION	TLB	SJC	
1	OCT 15/25	FIRST SUBMISSION	TLB	SJC	
No.	DATE	DESCRIPTION	BY	APPD	
REVISION / ISSUE					

Seal not valid unless signed and dated

U:\Masters Documents\ CIV 01 20\Bakr, Elwan A\Public 45469000704 Drafts\Turbines Desc. Plan 2008.05.23.dwg Lin 03 2008 40.58.22

H:\Master Documents_CIVIL_30\Bak Fire\Ac\Pub\sh_154688\00704 Dry Drive Townhouse Base Plan 2026-05-22.dwg Jun 02, 2026 - 10:58am



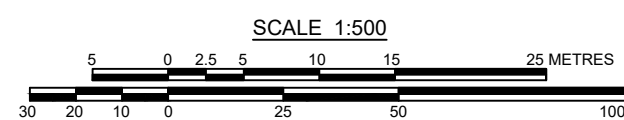
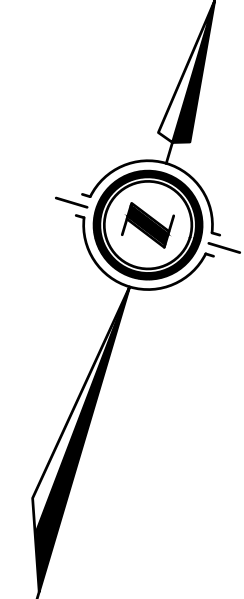
LEGEND

- | | | | | | | | |
|-------|---------------------------|---|-------|--|---|------|---------------------------------|
| ----- | PROPERTY BOUNDARY | ● | SANMH | PROPOSED SANITARY MANHOLE | □ | CB | PROPOSED CATCH BASIN |
| ----- | EDGE OF EXISTING PAVEMENT | ○ | STMMH | EXISTING SANITARY MANHOLE | □ | DICB | EXISTING CATCH BASIN |
| ----- | EDGE OF EXISTING GRAVEL | ○ | STMMH | PROPOSED STORM MANHOLE | □ | DICB | PROPOSED DITCH INLET CATCHBASIN |
| ----- | PROPOSED SANITARY SEWER | ○ | STMMH | EXISTING STORM MANHOLE | □ | DICB | PROPOSED HYDRANT SET |
| ----- | EXISTING SANITARY SEWER | ○ | STMMH | PROPOSED CATCHBASIN MANHOLE | □ | DICB | EXISTING FIRE HYDRANT |
| ----- | PROPOSED STORM SEWER | ○ | STMMH | PROPOSED TWIN INLET CATCHBASIN MANHOLE | □ | DICB | PROPOSED GATE VALVE |
| ----- | EXISTING STORM SEWER | ○ | STMMH | PROPOSED TWIN INLET CATCHBASIN | □ | DICB | EXISTING GATE VALVE |
| ----- | PROPOSED SUBDRAIN | ○ | STMMH | PROPOSED LIGHT POLE | □ | DICB | PROPOSED BEND c/w RESTRAINTS |
| ----- | PROPOSED WATERMAIN | ○ | STMMH | | □ | DICB | |
| ----- | EXISTING WATERMAIN | ○ | STMMH | | □ | DICB | |

CAUTION:
THE POSITION OF POLE LINES, CONDUITS, WATERMANS, SEWERS AND OTHER UNDERGROUND AND OVERGROUND UTILITIES AND STRUCTURES IS NOT NECESSARILY SHOWN ON THE DRAWINGS, AND, WHERE SHOWN, THE ACCURACY OF THE POSITION OF SUCH UTILITIES AND STRUCTURES IS NOT GUARANTEED. BEFORE STARTING WORK, THE CONTRACTOR SHALL INFORM HIMSELF OF THE EXACT LOCATION OF ALL SUCH UTILITIES AND STRUCTURES, AND SHALL ASSUME ALL LIABILITY FOR DAMAGE TO THEM.

Notes

1. PROPERTY BOUNDARY DERIVED FROM PLAN OF SURVEY BY ZUBEK, EMO, PATTEN AND THOMSEN LTD.
2. SEE SHEET 00704-DET1 FOR TYPICAL CROSS SECTION AND PAVEMENT DESIGN.
3. ALL ORGANIC MATERIAL WITHIN 1.2m OF FINISHED PROFILE GRADE TO BE REMOVED FROM ALL AREAS UNDER THE TRAVELLED PORTION OF THE ROAD.
4. COVER OVER WATERMAIN 1.7m MINIMUM AT ALL POINTS.
5. SANITARY SEWER TO BE PVC SDR35.
6. ALL JOINTS OF SANITARY MANHOLES TO BE CAULKED WITH MIN. 15mm BEAD, INSTALLED ON THE TOP OF JOINT OF EACH SECTION PRIOR TO SECTION ABOVE BEING INSTALLED. CAULKING TO BE SIKAFLEX 1A OR APPROVED EQUIVALENT.
7. ALL HYDRANT SETS REQUIRE TEST POINT AND HYDRANT MARKER.
8. ALL STORM CATCHBASINS TO HAVE A MINIMUM SUMP OF 600mm AND ALL STORM MANHOLES TO HAVE A MINIMUM SUMP OF 300mm.
9. STORM SEWERS TO BE HDPE.
10. ALL DITCH INLET CATCHBASINS TO HAVE 3:1 GRATE (UNLESS OTHERWISE INDICATED).
11. ALL CATCHBASIN MANHOLE STRUCTURES TO BE 1200mmØ UNLESS OTHERWISE SHOWN.
12. ALL WATERMANS TO BE PVC WITH 20mmØ MUNICIPEX WATER SERVICES.
13. THIS DRAWING IS NOT TO BE USED FOR CONSTRUCTION PURPOSES UNTIL STAMPED 'ISSUED FOR CONSTRUCTION'.
14. ALL CONSTRUCTION TO BE COMPLETED TO MUNICIPAL SERVICING STANDARDS FOR THE TOWN OF COLLINGWOOD.

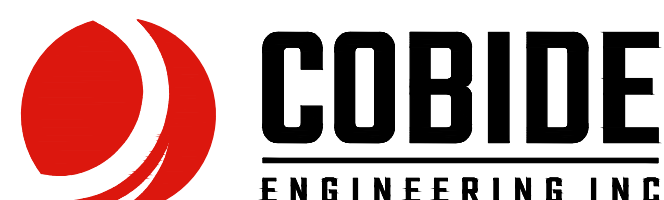


Benchmark Information

- | | | | |
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No.	DATE	DESCRIPTION	BY	APPD
4	JUN 02/26	THIRD SUBMISSION	TLB	SJC
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REVISION / ISSUE				

Seal not valid unless signed and dated



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PROPOSED TOWNHOUSE DEVELOPMENT TOWN OF COLLINGWOOD PRETTY RIVER ESTATES SITE SERVICING PLAN

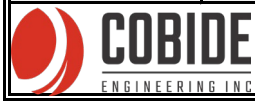
Client:	SUNVALE HOMES LTD.		
Design:	TLB	Scale:	1:500
Drawn:	ID	Approved:	
Checked:	TLB		
Date:	JUNE 2026		Design Engineer
DRAWING No.	00704-C5		

Appendix B

DESIGN SHEETS

FUNCTIONAL SERVICING REPORT

**DEY DRIVE TOWNHOUSES
TOWN OF COLLINGWOOD**

q = average daily per capita flow (260 L/cap.d) Where i = unit of peak extraneous flow (0.23 L/ha.s) M = peaking factor Q(p) = peak population (L/s) Q(i) = peak extraneous flow (L/s) Q(d) = peak design flow (L/s) Residential Density = 2.4 People per Dwelling Unit Residential Flow = 0.003 l/s/capita 260 l/day/ capita								SANITARY SEWER DESIGN SHEET						Q(p) = $\frac{PqM}{86.4}$ Q(i) = iA where A = area in hectares Q(d) = Q(p) + Q(i) (L/s)					
LOCATION			COM, IND, INST,			RESIDENTIAL		CUMULATIVE		Peaking Factor M	Pop. Flow Q(p) (L/s)	Peak Extraneous Q(i)	Peak Design Flow (L/s)	PROPOSED SEWER					
Street	From	To	Type	Flow (L/s/ha)	Area (hectares)	Pop.	Area (ha)	Pop.	Area (ha)					Length (m)	Pipe Size (mm)	Type of Pipe	Grade %	Capacity (L/s) n=0.013	Full Flow Velocity (m/s)
DEY DRIVE	SANMH1	SANMH2				12	0.22	12	0.22	4.41	0.16	0.05	0.21	19.3	200	PVC	0.60	25.1	0.80
	SANMH2	SANMH3				22	0.66	34	0.88	4.35	0.44	0.20	0.65	102.1	200	PVC	0.50	22.9	0.73
	SANMH3	SANMH4				36	0.88	70	1.76	4.28	0.90	0.41	1.31	119.5	200	PVC	0.40	20.5	0.65
	SANMH4	EX.SANMH7				10	0.16	80	1.93	4.27	1.02	0.44	1.47	54.5	200	PVC	0.4	20.5	0.65
										Date: 2026-06-01				PROJECT NO.: 00704				1 of 1	

	SUBDIVISION Dey Drive Townhouses					STORM SEWER DESIGN SHEET 100 YEAR STORM					DESIGN PARAMETERS I = a / ((tc + b) ^c) a= 2193.1 b= 9.04 c= 0.8710					DESIGN STORM 1 in 100 Years MANNING'S n = 0.013 MINIMUM COVER: 0.9 m TIME OF ENTRY 10 min							
	DATE: June 1, 2026 DESIGNED BY: RVA CHECKED BY: TLB										FILE NUMBER: 00704												
LOCATION		DRAINAGE AREA								PIPE SELECTION							CAPACITY (%)	PROFILE			DEPTH OF COVER		
	FROM M.H.	TO M.H.	AREA (ha)	C	A x R (ha)	ACCUM. AREA (ha)	T of C (min)	I (mm/h)	Q (m3/s)	LENGTH (m)	PIPE SIZE (mm)	SLOPE %	CAP. (FULL) (m3/s)	VEL. (FULL) (m/S)	TIME OF FLOW (min)		FALL IN SEWER (m)	UPSTREAM GROUND (m)	INVERT (m)	DOWNSTREAM INVERT (m)	DROP (m)	m	
101	DICB1	CBMH1	0.180	0.280	0.05	0.05	10.00	168.45	0.024	28.8	300	0.50	0.068	0.97	0.50	34.49%	0.14	193.81	193.16	193.02	0.08	0.35	
	CBMH1	TICBMH1	0.000	0.000	0.00	0.05	10.50	164.72	0.023	22.7	300	0.50	0.068	0.97	0.39	33.72%	0.11	194.52	192.94	192.82	0.18	1.28	
						TOTAL	10.89																
102	TICB1	TICBMH1	0.151	0.710	0.11	0.11	10.00	168.45	0.050	8.5	300	1.00	0.097	1.37	0.10	51.84%	0.09	194.36	192.86	192.78		1.20	
						TOTAL	10.10																
103	TICBMH1	TICBMH2	0.041	0.540	0.02	0.18	10.89	161.90	0.081	51.8	375	0.50	0.124	1.12	0.77	65.15%	0.26	194.30	192.66	192.40	0.03	1.27	
						TOTAL	11.66																
104	DICB2	DICB3	0.031	0.420	0.01	0.01	10.00	168.45	0.006	8.3	300	0.50	0.068	0.97	0.14	9.02%	0.04	194.15	192.91	192.87		0.94	
105	DICB3	DICB4	0.046	0.200	0.01	0.01	10.14	167.35	0.004	37.0	300	0.50	0.068	0.97	0.64	6.31%	0.19	194.01	193.20	193.02	0.05	0.51	
106	DICB4	DICB5	0.128	0.420	0.05	0.06	10.78	162.66	0.028	54.7	300	0.50	0.068	0.97	0.94	41.54%	0.27	194.07	192.97	192.69	0.08	0.81	
107	DICB5	TICBMH3	0.120	0.490	0.06	0.12	11.72	156.21	0.053	38.7	300	0.50	0.068	0.97	0.67	77.15%	0.19	194.05	192.61	192.42		1.14	
108	TICBMH3	TICBMH2	0.143	0.740	0.11	0.23	12.39	151.96	0.096	8.5	375	1.00	0.175	1.59	0.09	54.81%	0.09	194.27	192.77	192.69		1.13	
						TOTAL	12.48																
109	TICBMH2	TICBMH5	0.098	0.490	0.05	0.46	12.48	151.42	0.191	65.6	525	0.50	0.304	1.40	0.78	62.97%	0.33	194.27	192.31	191.98	0.03	1.44	
						TOTAL	13.26																
110	DICB6	TICBMH4	0.173	0.520	0.09	0.09	10.00	168.45	0.042	39.3	300	0.50	0.068	0.97	0.68	61.52%	0.20	193.75	192.25	192.05		1.20	
111	TICBMH4	TICBMH5	0.141	0.700	0.10	0.19	10.68	163.40	0.086	8.5	300	1.20	0.106	1.50	0.09	80.77%	0.10	194.16	192.66	192.56		1.20	
						TOTAL	10.77																
112	TICBMH5	TICBMH6	0.101	0.480	0.05	0.69	13.26	146.80	0.282	53.3	600	0.50	0.434	1.54	0.58	65.02%	0.27	194.16	191.95	191.69	0.03	1.61	
						TOTAL	13.84																
113	TICB4	TICBMH6	0.219	0.710	0.16	0.16	10.00	168.45	0.073	8.5	300	1.00	0.097	1.37	0.10	75.20%	0.09	194.09	192.59	192.51		1.20	
						TOTAL	10.10	167.66															
114	TICBMH6	STMMH1	0.119	0.550	0.07	0.91	13.84	143.57	0.364	38.0	675	0.50	0.594	1.66	0.38	61.26%	0.19	194.09	191.66	191.47	0.08	1.76	
						TOTAL	14.22																
115	DICB7	DICB8	0.056	0.450	0.03	0.03	10.00	168.45	0.012	15.1	300	0.50	0.068	0.97	0.26	17.19%	0.08	193.93	192.44	192.36	0.08	1.19	
116	DICB8	STMMH1	0.023	0.200	0.00	0.03	10.26	166.47	0.014	38.1	300	0.50	0.068	0.97	0.66	20.04%	0.19	193.70	192.28	192.09		1.12	
						TOTAL	10.92																
	STMMH1	CBMH2	0.000	0.000	0.00	0.94	14.22	141.51	0.371	6.7	675	0.50	0.594	1.66	0.07	62.35%	0.03	194.36	191.39	191.35	0.03	2.30	
						TOTAL	14.28																
117	DICB9	DICB10	0.045	0.510	0.02	0.02	10.00	168.45	0.011	34.9	300	0.50	0.068	0.97	0.60	15.78%	0.17	194.27	192.77	192.60	0.08	1.20	
118	DICB10	DICB11	0.029	0.440	0.01	0.04	10.60	163.95	0.016	31.3	300	0.50	0.068	0.97	0.54	23.98%	0.16	194.23	192.52	192.36	0.03	1.41	
119	DICB11	CBMH2	0.012	0.200	0.00	0.04	11.14	160.13	0.017	12.1	300	2.00	0.137	1.93	0.10	12.50%	0.24	194.19	192.33	192.09		1.56	
						TOTAL	11.24																
120	CBMH2	STMMH2	0.052	0.730	0.04	1.02	14.28	141.16	0.400	36.6	675	0.50	0.594	1.66	0.37	67.25%	0.18	194.05	191.32	191.14	0.03	2.05	
	STMMH2	STMMH3	0.000	0.000	0.00	1.02	14.65	139.25	0.394	37.6	675	0.50	0.594	1.66	0.38	66.34%	0.19	192.61	191.11	190.92	0.08	0.83	
	STMMH3	POND	0.000	0.000	0.00	1.02	15.03	137.35	0.389	40.1	675	0.50	0.594	1.66	0.40	65.44%	0.20	193.36	190.84	190.64		1.84	
						TOTAL	15.43																

Post Development Runoff Coefficients

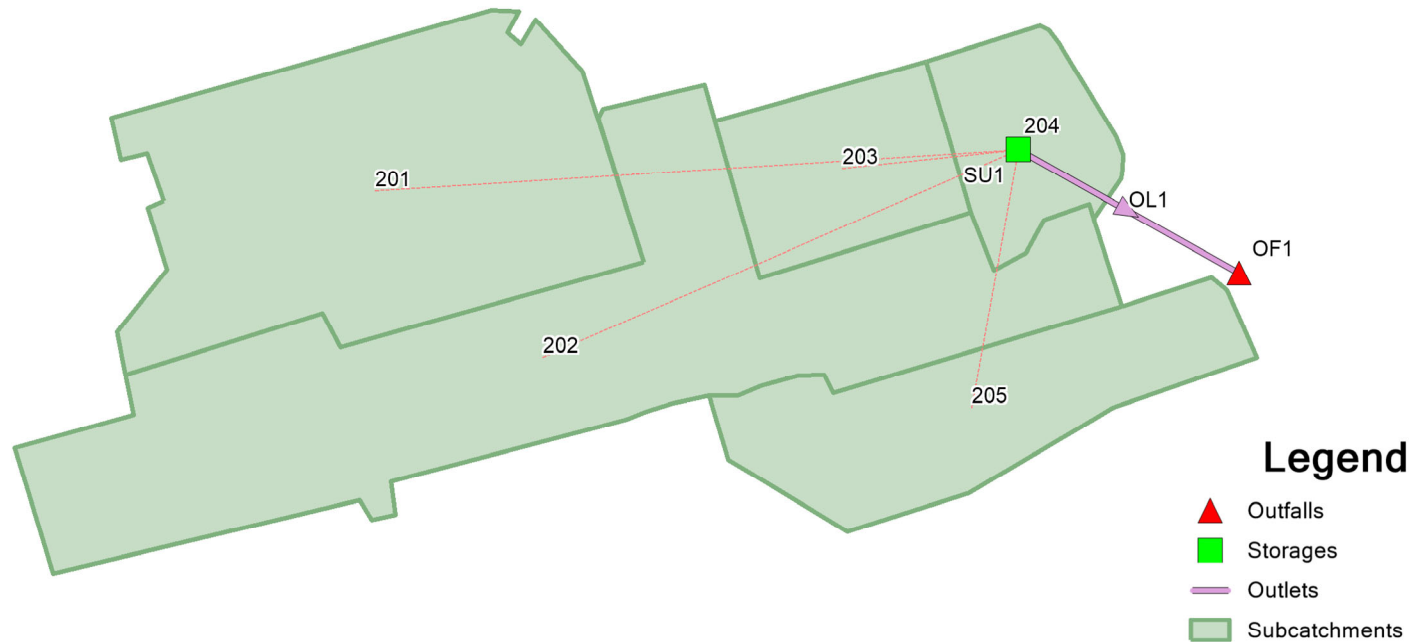
Appendix C

SWM MODELLING

FUNCTIONAL SERVICING REPORT

**DEY DRIVE TOWNHOUSES
TOWN OF COLLINGWOOD**

DEY DRIVE TOWNHOUSES - SWM MODEL SCHEMATIC



DEY DRIVE TOWNHOUSES – SWM MODELLING – MODEL DETAILS

[TITLE]

```
;;Project Title/Notes
```

[OPTIONS]

```
;;Option      Value
FLOW_UNITS    CMS
INFILTRATION  HORTON
FLOW_ROUTING  DYNWAVE
LINK_OFFSETS  DEPTH
MIN_SLOPE     0
ALLOW_PONDING NO
SKIP_STEADY_STATE NO

START_DATE    10/13/2025
START_TIME    00:00:00
REPORT_START_DATE 10/13/2025
REPORT_START_TIME 00:00:00
END_DATE      10/14/2025
END_TIME      00:00:00
SWEEP_START   1/1
SWEEP_END     12/31
DRY_DAYS      0
REPORT_STEP   00:01:00
WET_STEP      00:05:00
DRY_STEP      00:05:00
ROUTING_STEP  5
RULE_STEP     00:00:00

INERTIAL_DAMPING PARTIAL
NORMAL_FLOW_LIMITED BOTH
FORCE_MAIN_EQUATION H-W
VARIABLE_STEP    0.75
LENGTHENING_STEP 0
MIN_SURFAREA     0
MAX_TRIALS       8
HEAD_TOLERANCE   0
SYS_FLOW_TOL     5
LAT_FLOW_TOL     5
MINIMUM_STEP     0.5
THREADS          16
```

[EVAPORATION]

```
;;Data Source Parameters
;;-----
CONSTANT      0.0
DRY_ONLY      NO
```

[RAINGAGES]

```
;;Name      Format      Interval SCF      Source
;;-----
Chicago_4h_100yr VOLUME  0:05    1.0    TIMESERIES Chicago_4h_100yr
Chicago_4h_25yr  VOLUME  0:05    1.0    TIMESERIES Chicago_4h_25yr
Chicago_4h_2yr   VOLUME  0:05    1.0    TIMESERIES Chicago_4h_2yr
Chicago_4h_50yr  VOLUME  0:05    1.0    TIMESERIES Chicago_4h_50yr
Chicago_4h_5yr   VOLUME  0:05    1.0    TIMESERIES Chicago_4h_5yr
SCS_Type_II_46.8mm_2yr_24hr_Collingwood INTENSITY 0:06    1.0    TIMESERIES SCS_Type_II_46.8mm_2yr_24hr_Collingwood
SCS_Type_II_60.3mm_5yr_24hr_Collingwood INTENSITY 0:06    1.0    TIMESERIES SCS_Type_II_60.3mm_5yr_24hr_Collingwood
SCS_Type_II_80.5mm_25yr_24hr_Collingwood INTENSITY 0:06    1.0    TIMESERIES SCS_Type_II_80.5mm_25yr_24hr_Collingwood
SCS_Type_II_88.8mm_50yr_24hr_Collingwood INTENSITY 0:06    1.0    TIMESERIES SCS_Type_II_88.8mm_50yr_24hr_Collingwood
SCS_Type_II_97.1mm_100yr_24hr_Collingwood INTENSITY 0:06    1.0    TIMESERIES SCS_Type_II_97.1mm_100yr_24hr_Collingwood
```

[SUBCATCHMENTS]

```
;;Name      Rain Gage      Outlet      Area      %Imperv Width      %Slope CurbLen      SnowPack
;;-----
201         Chicago_4h_100yr SU1      4.64      50      264      2      0
202         Chicago_4h_100yr SU1      6.71      50      314      2      0
203         Chicago_4h_100yr SU1      1.27      0       138      2      0
204         Chicago_4h_100yr SU1      1.07      50      400      2      0
205         Chicago_4h_100yr SU1      1.9       50      750      2      0
```

[SUBAREAS]

```
;;Subcatchment N-Imperv N-Perv S-Imperv S-Perv PctZero RouteTo PctRouted
;;-----
```

DEY DRIVE TOWNHOUSES – SWM MODELLING – MODEL DETAILS

201	0.013	0.15	0.05	0.05	25	OUTLET
202	0.013	0.15	0.05	0.05	25	OUTLET
203	0.013	0.15	0.05	0.05	25	OUTLET
204	0.013	0.15	0.05	0.05	25	OUTLET
205	0.013	0.15	0.05	0.05	25	OUTLET

[INFILTRATION]

;;Subcatchment	Param1	Param2	Param3	Param4	Param5	
;;-----						
201	68	0.5	7	0	0	CURVE_NUMBER
202	68	0.5	7	0	0	CURVE_NUMBER
203	68	0.5	7	0	0	CURVE_NUMBER
204	68	0.5	7	0	0	CURVE_NUMBER
205	68	0.5	7	0	0	CURVE_NUMBER

[OUTFALLS]

;;Name	Elevation	Type	Stage Data	Gated	Route To
;;-----					
OF1	0	FREE		NO	

[STORAGE]

;;Name	Elev.	MaxDepth	InitDepth	Shape	Curve Name/Params	SurDepth	Fevap	Psi	Ksat	IMD
;;-----										
SU1	189.6	3.9	1	TABULAR	Eden_Oak_East_Pond	0	0			

[OUTLETS]

;;Name	From Node	To Node	Offset	Type	QTable/Qcoeff	Qexpon	Gated
;;-----							
OL1	SU1	OF1	0	TABULAR/HEAD	Outlet		NO

[CURVES]

;;Name	Type	X-Value	Y-Value
;;-----			
Outlet	Rating	0	0
Outlet		1	0
Outlet		1.1	0.011
Outlet		1.2	0.016
Outlet		1.3	0.019
Outlet		1.4	0.022
Outlet		1.5	0.0245
Outlet		1.6	0.0265
Outlet		1.7	0.0285
Outlet		1.8	0.03
Outlet		1.9	0.0315
Outlet		2	0.033
Outlet		2.1	0.0345
Outlet		2.2	0.0365
Outlet		2.3	0.038
Outlet		2.4	0.0395
Outlet		2.5	0.041
Outlet		2.6	0.0425
Outlet		2.7	0.044
Outlet		2.8	0.4019
Outlet		2.9	0.4687
Outlet		3	0.5255
Outlet		3.1	0.5763
Outlet		3.2	0.6227
Outlet		3.3	0.6656
Outlet		3.4	0.7058
Outlet		3.5	0.905
Outlet		3.6	1.2359
Outlet		3.7	1.6521
Outlet		3.8	2.1372
Outlet		3.9	2.6817

Eden_Oak_East_Pond	Storage	0	1080.56
Eden_Oak_East_Pond		0.3	1266.73
Eden_Oak_East_Pond		0.4	1333.95
Eden_Oak_East_Pond		0.6	1471.19
Eden_Oak_East_Pond		0.7	1541.2
Eden_Oak_East_Pond		0.8	3240.68
Eden_Oak_East_Pond		0.9	3420.18

DEY DRIVE TOWNHOUSES – SWM MODELLING – MODEL DETAILS

Eden_Oak_East_Pond	1	3551.17
Eden_Oak_East_Pond	1.1	3741.96
Eden_Oak_East_Pond	1.2	3876.5
Eden_Oak_East_Pond	1.3	4019.66
Eden_Oak_East_Pond	1.4	4144.23
Eden_Oak_East_Pond	1.5	4270.48
Eden_Oak_East_Pond	1.6	4398.41
Eden_Oak_East_Pond	1.7	4528.01
Eden_Oak_East_Pond	1.8	4659.3
Eden_Oak_East_Pond	1.9	4792.26
Eden_Oak_East_Pond	2	4926.89
Eden_Oak_East_Pond	2.1	5063.21
Eden_Oak_East_Pond	2.2	5201.2
Eden_Oak_East_Pond	2.3	5340.87
Eden_Oak_East_Pond	2.4	5482.22
Eden_Oak_East_Pond	2.5	5626.49
Eden_Oak_East_Pond	2.6	5773
Eden_Oak_East_Pond	2.7	5922.29
Eden_Oak_East_Pond	2.8	6073.48
Eden_Oak_East_Pond	2.9	6226.85
Eden_Oak_East_Pond	3	6382.42
Eden_Oak_East_Pond	3.1	6541.59
Eden_Oak_East_Pond	3.2	6705.95
Eden_Oak_East_Pond	3.3	6874.6
Eden_Oak_East_Pond	3.4	7047.55
Eden_Oak_East_Pond	3.5	7248.97
Eden_Oak_East_Pond	3.6	7429.63
Eden_Oak_East_Pond	3.7	7592.43
Eden_Oak_East_Pond	3.8	7781.22
Eden_Oak_East_Pond	3.9	7975.04

[TIMESERIES]

```
;;Name      Date      Time      Value
;-----
;Chicago design storm, a = 2193.1, b = 9.04, c = 0.871, Duration = 240 minutes, r = 0.35, rain interval = 5 minutes, rain units
= mm.
Chicago_4h_100yr

;Chicago design storm, a = 1676.2, b = 8.3, c = 0.858, Duration = 240 minutes, r = 0.35, rain interval = 5 minutes, rain units =
mm.
Chicago_4h_25yr

;Chicago design storm, a = 807.44, b = 6.75, c = 0.828, Duration = 240 minutes, r = 0.35, rain interval = 5 minutes, rain units
= mm.
Chicago_4h_2yr

;Chicago design storm, a = 1973.1, b = 9, c = 0.868, Duration = 240 minutes, r = 0.35, rain interval = 5 minutes, rain units =
mm.
Chicago_4h_50yr

;Chicago design storm, a = 1135.4, b = 7.5, c = 0.841, Duration = 240 minutes, r = 0.35, rain interval = 5 minutes, rain units =
mm.
Chicago_4h_5yr

;SCS_Type II_46.8mm design storm, total rainfall = 46.8 mm, rain interval = 6 minutes, rain units = mm/hr.
SCS_Type_II_46.8mm_2yr_24hr_Collingwood

;SCS_Type II_60.3mm design storm, total rainfall = 60.3 mm, rain interval = 6 minutes, rain units = mm/hr.
SCS_Type_II_60.3mm_5yr_24hr_Collingwood

;SCS_Type II_80.5mm design storm, total rainfall = 80.5 mm, rain interval = 6 minutes, rain units = mm/hr.
SCS_Type_II_80.5mm_25yr_24hr_Collingwood

;SCS_Type II_88.8mm design storm, total rainfall = 88.8 mm, rain interval = 6 minutes, rain units = mm/hr.
SCS_Type_II_88.8mm_50yr_24hr_Collingwood

;SCS_Type II_97.1mm design storm, total rainfall = 97.1 mm, rain interval = 6 minutes, rain units = mm/hr.
SCS_Type_II_97.1mm_100yr_24hr_Collingwood
```

[REPORT]

```
;;Reporting Options
INPUT      YES
CONTROLS   NO
```

DEY DRIVE TOWNHOUSES – SWM MODELLING – MODEL DETAILS

SUBCATCHMENTS ALL
NODES ALL
LINKS ALL

[TAGS]

[MAP]

DIMENSIONS	-8928805.6335	5540482.45755	-8927641.5145	5541010.26945
UNITS	Meters			

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 2 YEAR STORM EVENT

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.2 (Build 5.2.4)

Element Count

Number of rain gages 10
 Number of subcatchments ... 5
 Number of nodes 2
 Number of links 1
 Number of pollutants 0
 Number of land uses 0

Raingage Summary

Name	Data Source	Data Type	Recording Interval
Chicago_4h_100yr	Chicago_4h_100yr	VOLUME	5 min.
Chicago_4h_25yr	Chicago_4h_25yr	VOLUME	5 min.
Chicago_4h_2yr	Chicago_4h_2yr	VOLUME	5 min.
Chicago_4h_50yr	Chicago_4h_50yr	VOLUME	5 min.
Chicago_4h_5yr	Chicago_4h_5yr	VOLUME	5 min.
SCS_Type_II_46.8mm_2yr_24hr_Collingwood	SCS_Type_II_46.8mm_2yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_60.3mm_5yr_24hr_Collingwood	SCS_Type_II_60.3mm_5yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_80.5mm_25yr_24hr_Collingwood	SCS_Type_II_80.5mm_25yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_88.8mm_50yr_24hr_Collingwood	SCS_Type_II_88.8mm_50yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_97.1mm_100yr_24hr_Collingwood	SCS_Type_II_97.1mm_100yr_24hr_Collingwood	INTENSITY	6 min.

Subcatchment Summary

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
201	4.64	264.00	50.00	2.0000	Chicago_4h_2yr	SU1
202	6.71	314.00	50.00	2.0000	Chicago_4h_2yr	SU1
203	1.27	138.00	0.00	2.0000	Chicago_4h_2yr	SU1
204	1.07	400.00	50.00	2.0000	Chicago_4h_2yr	SU1
205	1.90	750.00	50.00	2.0000	Chicago_4h_2yr	SU1

Node Summary

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
OF1	OUTFALL	0.00	0.00	0.0	
SU1	STORAGE	189.60	3.90	0.0	

Link Summary

Name	From Node	To Node	Type	Length	%Slope	Roughness
OL1	SU1	OF1	OUTLET			

Cross Section Summary

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 2 YEAR STORM EVENT

Analysis Options

Flow Units CMS

Process Models:

Rainfall/Runoff YES
 RDII NO
 Snowmelt NO
 Groundwater NO
 Flow Routing YES
 Ponding Allowed NO
 Water Quality NO
 Infiltration Method HORTON
 Flow Routing Method DYNWAVE
 Surcharge Method EXTRAN
 Starting Date 10/13/2025 00:00:00
 Ending Date 10/14/2025 00:00:00
 Antecedent Dry Days 0.0
 Report Time Step 00:01:00
 Wet Time Step 00:05:00
 Dry Time Step 00:05:00
 Routing Time Step 5.00 sec
 Variable Time Step YES
 Maximum Trials 8
 Number of Threads 1
 Head Tolerance 0.001524 m

*****	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*****	-----	-----
Total Precipitation	0.526	33.759
Evaporation Loss	0.000	0.000
Infiltration Loss	0.225	14.459
Surface Runoff	0.302	19.356
Final Storage	0.001	0.081
Continuity Error (%)	-0.405	

*****	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.302	3.018
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	0.194	1.942
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.183	1.834
Final Stored Volume	0.291	2.910
Continuity Error (%)	0.002	

Time-Step Critical Elements

None

Highest Flow Instability Indexes

All links are stable.

Most Frequent Nonconverging Nodes

Convergence obtained at all time steps.

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 2 YEAR STORM EVENT

Routing Time Step Summary

```

Minimum Time Step      :    4.50 sec
Average Time Step      :    5.00 sec
Maximum Time Step      :    5.00 sec
% of Time in Steady State :    0.00
Average Iterations per Step :    2.00
% of Steps Not Converging :    0.00
Time Step Frequencies :
    5.000 - 3.155 sec :   100.00 %
    3.155 - 1.991 sec :    0.00 %
    1.991 - 1.256 sec :    0.00 %
    1.256 - 0.792 sec :    0.00 %
    0.792 - 0.500 sec :    0.00 %
  
```

Subcatchment Runoff Summary

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10 ⁶ ltr	Peak Runoff CMS	Runoff Coeff
201	33.76	0.00	0.00	13.37	17.03	3.45	20.48	0.95	0.58	0.607
202	33.76	0.00	0.00	13.46	17.03	3.36	20.38	1.37	0.80	0.604
203	33.76	0.00	0.00	26.75	0.00	6.90	6.90	0.09	0.01	0.204
204	33.76	0.00	0.00	13.16	16.90	3.71	20.61	0.22	0.16	0.611
205	33.76	0.00	0.00	13.16	16.90	3.71	20.61	0.39	0.29	0.610

Node Depth Summary

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
OF1	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
SU1	STORAGE	1.45	1.65	191.25	0 04:14	1.65

Node Inflow Summary

Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10 ⁶ ltr	Total Inflow Volume 10 ⁶ ltr	Flow Balance Error Percent
OF1	OUTFALL	0.000	0.028	0 04:14	0	1.94	0.000
SU1	STORAGE	1.843	1.843	0 01:25	3.02	4.85	0.002

Node Surcharge Summary

No nodes were surcharged.

Node Flooding Summary

No nodes were flooded.

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 2 YEAR STORM EVENT

Storage Volume Summary

Storage Unit	Average Volume 1000 m³	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m³	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CMS
SU1	3.618	19.9	0.0	0.0	4.465	24.6	0 04:14	0.028

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr
OF1	99.55	0.023	0.028	1.942
System	99.55	0.023	0.028	1.942

Link Flow Summary

Link	Type	Maximum Flow CMS	Time of Max Occurrence days hr:min	Maximum Veloc m/sec	Max/ Full Flow	Max/ Full Depth
OL1	DUMMY	0.028	0 04:14			

Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class							
		Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Tue Oct 14 20:46:43 2025
Analysis ended on: Tue Oct 14 20:46:43 2025
Total elapsed time: < 1 sec

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 5 YEAR STORM EVENT

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.2 (Build 5.2.4)

Element Count

Number of rain gages 10
 Number of subcatchments ... 5
 Number of nodes 2
 Number of links 1
 Number of pollutants 0
 Number of land uses 0

Raingage Summary

Name	Data Source	Data Type	Recording Interval
Chicago_4h_100yr	Chicago_4h_100yr	VOLUME	5 min.
Chicago_4h_25yr	Chicago_4h_25yr	VOLUME	5 min.
Chicago_4h_2yr	Chicago_4h_2yr	VOLUME	5 min.
Chicago_4h_50yr	Chicago_4h_50yr	VOLUME	5 min.
Chicago_4h_5yr	Chicago_4h_5yr	VOLUME	5 min.
SCS_Type_II_46.8mm_2yr_24hr_Collingwood	SCS_Type_II_46.8mm_2yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_60.3mm_5yr_24hr_Collingwood	SCS_Type_II_60.3mm_5yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_80.5mm_25yr_24hr_Collingwood	SCS_Type_II_80.5mm_25yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_88.8mm_50yr_24hr_Collingwood	SCS_Type_II_88.8mm_50yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_97.1mm_100yr_24hr_Collingwood	SCS_Type_II_97.1mm_100yr_24hr_Collingwood	INTENSITY	6 min.

Subcatchment Summary

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
201	4.64	264.00	50.00	2.0000	Chicago_4h_5yr	SU1
202	6.71	314.00	50.00	2.0000	Chicago_4h_5yr	SU1
203	1.27	138.00	0.00	2.0000	Chicago_4h_5yr	SU1
204	1.07	400.00	50.00	2.0000	Chicago_4h_5yr	SU1
205	1.90	750.00	50.00	2.0000	Chicago_4h_5yr	SU1

Node Summary

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
OF1	OUTFALL	0.00	0.00	0.0	
SU1	STORAGE	189.60	3.90	0.0	

Link Summary

Name	From Node	To Node	Type	Length	%Slope	Roughness
OL1	SU1	OF1	OUTLET			

Cross Section Summary

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 5 YEAR STORM EVENT

Analysis Options

Flow Units CMS

Process Models:

Rainfall/Runoff YES
 RDII NO
 Snowmelt NO
 Groundwater NO
 Flow Routing YES
 Ponding Allowed NO
 Water Quality NO
 Infiltration Method HORTON
 Flow Routing Method DYNWAVE
 Surcharge Method EXTRAN
 Starting Date 10/13/2025 00:00:00
 Ending Date 10/14/2025 00:00:00
 Antecedent Dry Days 0.0
 Report Time Step 00:01:00
 Wet Time Step 00:05:00
 Dry Time Step 00:05:00
 Routing Time Step 5.00 sec
 Variable Time Step YES
 Maximum Trials 8
 Number of Threads 1
 Head Tolerance 0.001524 m

*****	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*****	-----	-----
Total Precipitation	0.687	44.079
Evaporation Loss	0.000	0.000
Infiltration Loss	0.277	17.739
Surface Runoff	0.412	26.435
Final Storage	0.001	0.081
Continuity Error (%)	-0.402	

*****	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.412	4.121
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	0.229	2.294
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.183	1.834
Final Stored Volume	0.366	3.661
Continuity Error (%)	0.003	

Time-Step Critical Elements

None

Highest Flow Instability Indexes

All links are stable.

Most Frequent Nonconverging Nodes

Convergence obtained at all time steps.

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 5 YEAR STORM EVENT

Routing Time Step Summary

```

Minimum Time Step      :    4.50 sec
Average Time Step      :    5.00 sec
Maximum Time Step      :    5.00 sec
% of Time in Steady State :    0.00
Average Iterations per Step :    2.00
% of Steps Not Converging :    0.00
Time Step Frequencies :
    5.000 - 3.155 sec :   100.00 %
    3.155 - 1.991 sec :    0.00 %
    1.991 - 1.256 sec :    0.00 %
    1.256 - 0.792 sec :    0.00 %
    0.792 - 0.500 sec :    0.00 %
  
```

Subcatchment Runoff Summary

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10^6 ltr	Peak Runoff CMS	Runoff Coeff
201	44.08	0.00	0.00	16.42	22.23	5.57	27.80	1.29	0.79	0.631
202	44.08	0.00	0.00	16.52	22.23	5.46	27.70	1.86	1.09	0.628
203	44.08	0.00	0.00	32.85	0.00	11.13	11.13	0.14	0.02	0.252
204	44.08	0.00	0.00	16.10	22.06	5.95	28.01	0.30	0.22	0.635
205	44.08	0.00	0.00	16.10	22.06	5.95	28.01	0.53	0.39	0.635

Node Depth Summary

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
OF1	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
SU1	STORAGE	1.65	1.88	191.48	0 04:18	1.88

Node Inflow Summary

Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10^6 ltr	Total Inflow Volume 10^6 ltr	Flow Balance Error Percent
OF1	OUTFALL	0.000	0.031	0 04:18	0	2.29	0.000
SU1	STORAGE	2.494	2.494	0 01:25	4.12	5.96	0.003

Node Surcharge Summary

No nodes were surcharged.

Node Flooding Summary

No nodes were flooded.

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 5 YEAR STORM EVENT

Storage Volume Summary

Storage Unit	Average Volume 1000 m³	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m³	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CMS
SU1	4.477	24.6	0.0	0.0	5.514	30.3	0 04:18	0.031

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr
OF1	99.62	0.027	0.031	2.294
System	99.62	0.027	0.031	2.294

Link Flow Summary

Link	Type	Maximum Flow CMS	Time of Max Occurrence days hr:min	Maximum Veloc m/sec	Max/ Full Flow	Max/ Full Depth
OL1	DUMMY	0.031	0 04:18			

Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class							
		Up Dry	Down Dry	Sub Dry	Sup Crit	Up Crit	Down Crit	Norm Crit	Inlet Ltd
									Ctrl

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Tue Oct 14 20:48:37 2025
Analysis ended on: Tue Oct 14 20:48:37 2025
Total elapsed time: < 1 sec

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 25 YEAR STORM EVENT

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.2 (Build 5.2.4)

Element Count

Number of rain gages 10
 Number of subcatchments ... 5
 Number of nodes 2
 Number of links 1
 Number of pollutants 0
 Number of land uses 0

Raingage Summary

Name	Data Source	Data Type	Recording Interval
Chicago_4h_100yr	Chicago_4h_100yr	VOLUME	5 min.
Chicago_4h_25yr	Chicago_4h_25yr	VOLUME	5 min.
Chicago_4h_2yr	Chicago_4h_2yr	VOLUME	5 min.
Chicago_4h_50yr	Chicago_4h_50yr	VOLUME	5 min.
Chicago_4h_5yr	Chicago_4h_5yr	VOLUME	5 min.
SCS_Type_II_46.8mm_2yr_24hr_Collingwood	SCS_Type_II_46.8mm_2yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_60.3mm_5yr_24hr_Collingwood	SCS_Type_II_60.3mm_5yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_80.5mm_25yr_24hr_Collingwood	SCS_Type_II_80.5mm_25yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_88.8mm_50yr_24hr_Collingwood	SCS_Type_II_88.8mm_50yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_97.1mm_100yr_24hr_Collingwood	SCS_Type_II_97.1mm_100yr_24hr_Collingwood	INTENSITY	6 min.

Subcatchment Summary

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
201	4.64	264.00	50.00	2.0000	Chicago_4h_25yr	SU1
202	6.71	314.00	50.00	2.0000	Chicago_4h_25yr	SU1
203	1.27	138.00	0.00	2.0000	Chicago_4h_25yr	SU1
204	1.07	400.00	50.00	2.0000	Chicago_4h_25yr	SU1
205	1.90	750.00	50.00	2.0000	Chicago_4h_25yr	SU1

Node Summary

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
OF1	OUTFALL	0.00	0.00	0.0	
SU1	STORAGE	189.60	3.90	0.0	

Link Summary

Name	From Node	To Node	Type	Length	%Slope	Roughness
OL1	SU1	OF1	OUTLET			

Cross Section Summary

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 25 YEAR STORM EVENT

Analysis Options

Flow Units CMS

Process Models:

Rainfall/Runoff YES
 RDII NO
 Snowmelt NO
 Groundwater NO
 Flow Routing YES
 Ponding Allowed NO
 Water Quality NO
 Infiltration Method HORTON
 Flow Routing Method DYNWAVE
 Surcharge Method EXTRAN
 Starting Date 10/13/2025 00:00:00
 Ending Date 10/14/2025 00:00:00
 Antecedent Dry Days 0.0
 Report Time Step 00:01:00
 Wet Time Step 00:05:00
 Dry Time Step 00:05:00
 Routing Time Step 5.00 sec
 Variable Time Step YES
 Maximum Trials 8
 Number of Threads 1
 Head Tolerance 0.001524 m

*****	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*****	-----	-----
Total Precipitation	0.921	59.093
Evaporation Loss	0.000	0.000
Infiltration Loss	0.340	21.808
Surface Runoff	0.584	37.442
Final Storage	0.001	0.082
Continuity Error (%)	-0.405	

*****	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.584	5.837
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	0.271	2.712
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.183	1.834
Final Stored Volume	0.496	4.959
Continuity Error (%)	0.004	

Time-Step Critical Elements

None

Highest Flow Instability Indexes

All links are stable.

Most Frequent Nonconverging Nodes

Convergence obtained at all time steps.

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 25 YEAR STORM EVENT

Routing Time Step Summary

```

Minimum Time Step      :    4.50 sec
Average Time Step      :    5.00 sec
Maximum Time Step      :    5.00 sec
% of Time in Steady State :    0.00
Average Iterations per Step :    2.00
% of Steps Not Converging :    0.00
Time Step Frequencies :
    5.000 - 3.155 sec :   100.00 %
    3.155 - 1.991 sec :    0.00 %
    1.991 - 1.256 sec :    0.00 %
    1.256 - 0.792 sec :    0.00 %
    0.792 - 0.500 sec :    0.00 %
  
```

Subcatchment Runoff Summary

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10 ⁶ ltr	Peak Runoff CMS	Runoff Coeff
201	59.09	0.00	0.00	20.20	29.79	9.31	39.10	1.81	1.11	0.662
202	59.09	0.00	0.00	20.30	29.80	9.20	39.00	2.62	1.55	0.660
203	59.09	0.00	0.00	40.41	0.00	18.60	18.60	0.24	0.05	0.315
204	59.09	0.00	0.00	19.77	29.57	9.82	39.39	0.42	0.31	0.667
205	59.09	0.00	0.00	19.77	29.56	9.83	39.39	0.75	0.54	0.667

Node Depth Summary

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
OF1	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
SU1	STORAGE	1.94	2.21	191.81	0 04:20	2.21

Node Inflow Summary

Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10 ⁶ ltr	Total Inflow Volume 10 ⁶ ltr	Flow Balance Error Percent
OF1	OUTFALL	0.000	0.037	0 04:20	0	2.71	0.000
SU1	STORAGE	3.521	3.521	0 01:25	5.84	7.67	0.004

Node Surcharge Summary

No nodes were surcharged.

Node Flooding Summary

No nodes were flooded.

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 25 YEAR STORM EVENT

Storage Volume Summary

Storage Unit	Average Volume 1000 m³	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m³	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CMS
SU1	5.863	32.3	0.0	0.0	7.161	39.4	0 04:20	0.037

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr
OF1	99.69	0.031	0.037	2.712
System	99.69	0.031	0.037	2.712

Link Flow Summary

Link	Type	Maximum Flow CMS	Time of Max Occurrence days hr:min	Maximum Veloc m/sec	Max/ Full Flow	Max/ Full Depth
OL1	DUMMY	0.037	0 04:20			

Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class							
		Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Tue Oct 14 20:48:00 2025
Analysis ended on: Tue Oct 14 20:48:00 2025
Total elapsed time: < 1 sec

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 50 YEAR STORM EVENT

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.2 (Build 5.2.4)

Element Count

Number of rain gages 10
 Number of subcatchments ... 5
 Number of nodes 2
 Number of links 1
 Number of pollutants 0
 Number of land uses 0

Raingage Summary

Name	Data Source	Data Type	Recording Interval
Chicago_4h_100yr	Chicago_4h_100yr	VOLUME	5 min.
Chicago_4h_25yr	Chicago_4h_25yr	VOLUME	5 min.
Chicago_4h_2yr	Chicago_4h_2yr	VOLUME	5 min.
Chicago_4h_50yr	Chicago_4h_50yr	VOLUME	5 min.
Chicago_4h_5yr	Chicago_4h_5yr	VOLUME	5 min.
SCS_Type_II_46.8mm_2yr_24hr_Collingwood	SCS_Type_II_46.8mm_2yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_60.3mm_5yr_24hr_Collingwood	SCS_Type_II_60.3mm_5yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_80.5mm_25yr_24hr_Collingwood	SCS_Type_II_80.5mm_25yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_88.8mm_50yr_24hr_Collingwood	SCS_Type_II_88.8mm_50yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_97.1mm_100yr_24hr_Collingwood	SCS_Type_II_97.1mm_100yr_24hr_Collingwood	INTENSITY	6 min.

Subcatchment Summary

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
201	4.64	264.00	50.00	2.0000	Chicago_4h_50yr	SU1
202	6.71	314.00	50.00	2.0000	Chicago_4h_50yr	SU1
203	1.27	138.00	0.00	2.0000	Chicago_4h_50yr	SU1
204	1.07	400.00	50.00	2.0000	Chicago_4h_50yr	SU1
205	1.90	750.00	50.00	2.0000	Chicago_4h_50yr	SU1

Node Summary

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
OF1	OUTFALL	0.00	0.00	0.0	
SU1	STORAGE	189.60	3.90	0.0	

Link Summary

Name	From Node	To Node	Type	Length	%Slope	Roughness
OL1	SU1	OF1	OUTLET			

Cross Section Summary

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 50 YEAR STORM EVENT

Analysis Options

Flow Units CMS

Process Models:

Rainfall/Runoff YES
 RDII NO
 Snowmelt NO
 Groundwater NO
 Flow Routing YES
 Ponding Allowed NO
 Water Quality NO
 Infiltration Method HORTON
 Flow Routing Method DYNWAVE
 Surcharge Method EXTRAN
 Starting Date 10/13/2025 00:00:00
 Ending Date 10/14/2025 00:00:00
 Antecedent Dry Days 0.0
 Report Time Step 00:01:00
 Wet Time Step 00:05:00
 Dry Time Step 00:05:00
 Routing Time Step 5.00 sec
 Variable Time Step YES
 Maximum Trials 8
 Number of Threads 1
 Head Tolerance 0.001524 m

*****	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*****	-----	-----
Total Precipitation	1.024	65.662
Evaporation Loss	0.000	0.000
Infiltration Loss	0.364	23.379
Surface Runoff	0.662	42.460
Final Storage	0.001	0.082
Continuity Error (%)	-0.395	

*****	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.662	6.620
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	0.289	2.890
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.183	1.834
Final Stored Volume	0.556	5.563
Continuity Error (%)	0.005	

Time-Step Critical Elements

None

Highest Flow Instability Indexes

All links are stable.

Most Frequent Nonconverging Nodes

Convergence obtained at all time steps.

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 50 YEAR STORM EVENT

Routing Time Step Summary

```

Minimum Time Step      :    4.50 sec
Average Time Step      :    5.00 sec
Maximum Time Step      :    5.00 sec
% of Time in Steady State :    0.00
Average Iterations per Step :    2.00
% of Steps Not Converging :    0.00
Time Step Frequencies :
    5.000 - 3.155 sec :   100.00 %
    3.155 - 1.991 sec :    0.00 %
    1.991 - 1.256 sec :    0.00 %
    1.256 - 0.792 sec :    0.00 %
    0.792 - 0.500 sec :    0.00 %
  
```

Subcatchment Runoff Summary

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10 ⁶ ltr	Peak Runoff CMS	Runoff Coeff
201	65.66	0.00	0.00	21.66	33.09	11.14	44.23	2.05	1.24	0.674
202	65.66	0.00	0.00	21.76	33.11	11.03	44.13	2.96	1.73	0.672
203	65.66	0.00	0.00	43.33	0.00	22.27	22.27	0.28	0.06	0.339
204	65.66	0.00	0.00	21.19	32.85	11.71	44.56	0.48	0.34	0.679
205	65.66	0.00	0.00	21.19	32.85	11.71	44.56	0.85	0.61	0.679

Node Depth Summary

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
OF1	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
SU1	STORAGE	2.07	2.35	191.95	0 04:21	2.35

Node Inflow Summary

Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10 ⁶ ltr	Total Inflow Volume 10 ⁶ ltr	Flow Balance Error Percent
OF1	OUTFALL	0.000	0.039	0 04:21	0	2.89	0.000
SU1	STORAGE	3.938	3.938	0 01:25	6.62	8.45	0.005

Node Surcharge Summary

No nodes were surcharged.

Node Flooding Summary

No nodes were flooded.

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 50 YEAR STORM EVENT

Storage Volume Summary

Storage Unit	Average Volume 1000 m³	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m³	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CMS
SU1	6.498	35.7	0.0	0.0	7.915	43.5	0 04:21	0.039

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr
OF1	99.71	0.034	0.039	2.890
System	99.71	0.034	0.039	2.890

Link Flow Summary

Link	Type	Maximum Flow CMS	Time of Max Occurrence days hr:min	Maximum Veloc m/sec	Max/ Full Flow	Max/ Full Depth
OL1	DUMMY	0.039	0 04:21			

Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class							
		Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Tue Oct 14 20:49:06 2025
Analysis ended on: Tue Oct 14 20:49:06 2025
Total elapsed time: < 1 sec

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 100 YEAR STORM EVENT

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.2 (Build 5.2.4)

Element Count

Number of rain gages 10
 Number of subcatchments ... 5
 Number of nodes 2
 Number of links 1
 Number of pollutants 0
 Number of land uses 0

Raingage Summary

Name	Data Source	Data Type	Recording Interval
Chicago_4h_100yr	Chicago_4h_100yr	VOLUME	5 min.
Chicago_4h_25yr	Chicago_4h_25yr	VOLUME	5 min.
Chicago_4h_2yr	Chicago_4h_2yr	VOLUME	5 min.
Chicago_4h_50yr	Chicago_4h_50yr	VOLUME	5 min.
Chicago_4h_5yr	Chicago_4h_5yr	VOLUME	5 min.
SCS_Type_II_46.8mm_2yr_24hr_Collingwood	SCS_Type_II_46.8mm_2yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_60.3mm_5yr_24hr_Collingwood	SCS_Type_II_60.3mm_5yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_80.5mm_25yr_24hr_Collingwood	SCS_Type_II_80.5mm_25yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_88.8mm_50yr_24hr_Collingwood	SCS_Type_II_88.8mm_50yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_97.1mm_100yr_24hr_Collingwood	SCS_Type_II_97.1mm_100yr_24hr_Collingwood	INTENSITY	6 min.

Subcatchment Summary

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
201	4.64	264.00	50.00	2.0000	Chicago_4h_100yr	SU1
202	6.71	314.00	50.00	2.0000	Chicago_4h_100yr	SU1
203	1.27	138.00	0.00	2.0000	Chicago_4h_100yr	SU1
204	1.07	400.00	50.00	2.0000	Chicago_4h_100yr	SU1
205	1.90	750.00	50.00	2.0000	Chicago_4h_100yr	SU1

Node Summary

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
OF1	OUTFALL	0.00	0.00	0.0	
SU1	STORAGE	189.60	3.90	0.0	

Link Summary

Name	From Node	To Node	Type	Length	%Slope	Roughness
OL1	SU1	OF1	OUTLET			

Cross Section Summary

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 100 YEAR STORM EVENT

Analysis Options

Flow Units CMS

Process Models:

Rainfall/Runoff YES
 RDII NO
 Snowmelt NO
 Groundwater NO
 Flow Routing YES
 Ponding Allowed NO
 Water Quality NO
 Infiltration Method HORTON
 Flow Routing Method DYNWAVE
 Surcharge Method EXTRAN
 Starting Date 10/13/2025 00:00:00
 Ending Date 10/14/2025 00:00:00
 Antecedent Dry Days 0.0
 Report Time Step 00:01:00
 Wet Time Step 00:05:00
 Dry Time Step 00:05:00
 Routing Time Step 5.00 sec
 Variable Time Step YES
 Maximum Trials 8
 Number of Threads 1
 Head Tolerance 0.001524 m

*****	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*****	-----	-----
Total Precipitation	1.119	71.775
Evaporation Loss	0.000	0.000
Infiltration Loss	0.386	24.744
Surface Runoff	0.736	47.237
Final Storage	0.001	0.082
Continuity Error (%)	-0.401	

*****	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.736	7.364
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	0.305	3.053
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.183	1.834
Final Stored Volume	0.614	6.145
Continuity Error (%)	0.005	

Time-Step Critical Elements

None

Highest Flow Instability Indexes

All links are stable.

Most Frequent Nonconverging Nodes

Convergence obtained at all time steps.

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 100 YEAR STORM EVENT

Routing Time Step Summary

```

Minimum Time Step      :    4.50 sec
Average Time Step      :    5.00 sec
Maximum Time Step      :    5.00 sec
% of Time in Steady State :    0.00
Average Iterations per Step :    2.00
% of Steps Not Converging :    0.00
Time Step Frequencies :
    5.000 - 3.155 sec :   100.00 %
    3.155 - 1.991 sec :    0.00 %
    1.991 - 1.256 sec :    0.00 %
    1.256 - 0.792 sec :    0.00 %
    0.792 - 0.500 sec :    0.00 %
  
```

Subcatchment Runoff Summary

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10 ⁶ ltr	Peak Runoff CMS	Runoff Coeff
201	71.78	0.00	0.00	22.90	36.17	12.96	49.13	2.28	1.38	0.685
202	71.78	0.00	0.00	23.04	36.19	12.81	48.99	3.29	1.93	0.683
203	71.77	0.00	0.00	45.90	0.00	25.83	25.83	0.33	0.07	0.360
204	71.78	0.00	0.00	22.42	35.91	13.55	49.46	0.53	0.38	0.689
205	71.77	0.00	0.00	22.42	35.91	13.56	49.46	0.94	0.68	0.689

Node Depth Summary

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
OF1	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
SU1	STORAGE	2.19	2.48	192.08	0 04:22	2.48

Node Inflow Summary

Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10 ⁶ ltr	Total Inflow Volume 10 ⁶ ltr	Flow Balance Error Percent
OF1	OUTFALL	0.000	0.041	0 04:22	0	3.05	0.000
SU1	STORAGE	4.405	4.405	0 01:25	7.36	9.2	0.005

Node Surcharge Summary

No nodes were surcharged.

Node Flooding Summary

No nodes were flooded.

DEY DRIVE TOWNHOUSES – SWM MODELLING – CHICAGO 100 YEAR STORM EVENT

Storage Volume Summary

Storage Unit	Average Volume 1000 m³	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m³	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CMS
SU1	7.108	39.1	0.0	0.0	8.633	47.5	0 04:22	0.041

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr
OF1	99.73	0.035	0.041	3.053
System	99.73	0.035	0.041	3.053

Link Flow Summary

Link	Type	Maximum Flow CMS	Time of Max Occurrence days hr:min	Maximum Veloc m/sec	Max/ Full Flow	Max/ Full Depth
OL1	DUMMY	0.041	0 04:22			

Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class							
		Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Tue Oct 14 20:49:47 2025
Analysis ended on: Tue Oct 14 20:49:47 2025
Total elapsed time: < 1 sec

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 2 YEAR STORM EVENT

EPA STORM WATER MANAGEMENT MODEL – VERSION 5.2 (Build 5.2.4)

Element Count

Number of rain gages 10
 Number of subcatchments ... 5
 Number of nodes 2
 Number of links 1
 Number of pollutants 0
 Number of land uses 0

Raingage Summary

Name	Data Source	Data Type	Recording Interval
Chicago_4h_100yr	Chicago_4h_100yr	VOLUME	5 min.
Chicago_4h_25yr	Chicago_4h_25yr	VOLUME	5 min.
Chicago_4h_2yr	Chicago_4h_2yr	VOLUME	5 min.
Chicago_4h_50yr	Chicago_4h_50yr	VOLUME	5 min.
Chicago_4h_5yr	Chicago_4h_5yr	VOLUME	5 min.
SCS_Type_II_46.8mm_2yr_24hr_Collingwood	SCS_Type_II_46.8mm_2yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_60.3mm_5yr_24hr_Collingwood	SCS_Type_II_60.3mm_5yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_80.5mm_25yr_24hr_Collingwood	SCS_Type_II_80.5mm_25yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_88.8mm_50yr_24hr_Collingwood	SCS_Type_II_88.8mm_50yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_97.1mm_100yr_24hr_Collingwood	SCS_Type_II_97.1mm_100yr_24hr_Collingwood	INTENSITY	6 min.

Subcatchment Summary

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
201	4.64	264.00	50.00	2.0000	SCS_Type_II_46.8mm_2yr_24hr_Collingwood	SU1
202	6.71	314.00	50.00	2.0000	SCS_Type_II_46.8mm_2yr_24hr_Collingwood	SU1
203	1.27	138.00	0.00	2.0000	SCS_Type_II_46.8mm_2yr_24hr_Collingwood	SU1
204	1.07	400.00	50.00	2.0000	SCS_Type_II_46.8mm_2yr_24hr_Collingwood	SU1
205	1.90	750.00	50.00	2.0000	SCS_Type_II_46.8mm_2yr_24hr_Collingwood	SU1

Node Summary

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
OF1	OUTFALL	0.00	0.00	0.0	
SU1	STORAGE	189.60	3.90	0.0	

Link Summary

Name	From Node	To Node	Type	Length	%Slope	Roughness
OL1	SU1	OF1	OUTLET			

Cross Section Summary

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 2 YEAR STORM EVENT

Analysis Options

Flow Units CMS

Process Models:

Rainfall/Runoff YES
 RDII NO
 Snowmelt NO
 Groundwater NO
 Flow Routing YES
 Ponding Allowed NO
 Water Quality NO
 Infiltration Method HORTON
 Flow Routing Method DYNWAVE
 Surcharge Method EXTRAN
 Starting Date 10/13/2025 00:00:00
 Ending Date 10/14/2025 00:00:00
 Antecedent Dry Days 0.0
 Report Time Step 00:01:00
 Wet Time Step 00:05:00
 Dry Time Step 00:05:00
 Routing Time Step 5.00 sec
 Variable Time Step YES
 Maximum Trials 8
 Number of Threads 1
 Head Tolerance 0.001524 m

*****	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*****	-----	-----
Total Precipitation	0.730	46.800
Evaporation Loss	0.000	0.000
Infiltration Loss	0.284	18.186
Surface Runoff	0.438	28.113
Final Storage	0.009	0.569
Continuity Error (%)	-0.146	

*****	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.438	4.383
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	0.152	1.516
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.183	1.834
Final Stored Volume	0.470	4.701
Continuity Error (%)	0.005	

Time-Step Critical Elements

None

Highest Flow Instability Indexes

All links are stable.

Most Frequent Nonconverging Nodes

Convergence obtained at all time steps.

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 2 YEAR STORM EVENT

Routing Time Step Summary

```

Minimum Time Step      :    4.50 sec
Average Time Step      :    5.00 sec
Maximum Time Step      :    5.00 sec
% of Time in Steady State :    0.00
Average Iterations per Step :    2.00
% of Steps Not Converging :    0.00
Time Step Frequencies :
    5.000 - 3.155 sec :   100.00 %
    3.155 - 1.991 sec :    0.00 %
    1.991 - 1.256 sec :    0.00 %
    1.256 - 0.792 sec :    0.00 %
    0.792 - 0.500 sec :    0.00 %
  
```

Subcatchment Runoff Summary

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10 ⁶ ltr	Peak Runoff CMS	Runoff Coeff
201	46.80	0.00	0.00	16.82	23.32	6.16	29.48	1.37	0.41	0.630
202	46.80	0.00	0.00	16.82	23.30	6.11	29.40	1.97	0.57	0.628
203	46.80	0.00	0.00	33.63	0.00	12.30	12.30	0.16	0.02	0.263
204	46.80	0.00	0.00	16.82	23.38	6.44	29.83	0.32	0.11	0.637
205	46.80	0.00	0.00	16.82	23.38	6.45	29.83	0.57	0.20	0.637

Node Depth Summary

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
OF1	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
SU1	STORAGE	1.39	1.74	191.34	0 17:51	1.74

Node Inflow Summary

Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10 ⁶ ltr	Total Inflow Volume 10 ⁶ ltr	Flow Balance Error Percent
OF1	OUTFALL	0.000	0.029	0 17:51	0	1.52	0.000
SU1	STORAGE	1.307	1.307	0 11:54	4.38	6.22	0.005

Node Surcharge Summary

No nodes were surcharged.

Node Flooding Summary

No nodes were flooded.

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 2 YEAR STORM EVENT

Storage Volume Summary

Storage Unit	Average Volume 1000 m³	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m³	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CMS
SU1	3.410	18.8	0.0	0.0	4.880	26.8	0 17:51	0.029

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr
OF1	98.78	0.018	0.029	1.516
System	98.78	0.018	0.029	1.516

Link Flow Summary

Link	Type	Maximum Flow CMS	Time of Max Occurrence days hr:min	Maximum Veloc m/sec	Max/ Full Flow	Max/ Full Depth
OL1	DUMMY	0.029	0 17:51			

Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								
		Up		Down	Sub	Sup	Up	Down	Norm	Inlet
		Dry	Dry	Dry	Crit	Crit	Crit	Crit	Ltd	Ctrl

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Tue Oct 14 20:27:48 2025
Analysis ended on: Tue Oct 14 20:27:48 2025
Total elapsed time: < 1 sec

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 5 YEAR STORM EVENT

EPA STORM WATER MANAGEMENT MODEL – VERSION 5.2 (Build 5.2.4)

Element Count

Number of rain gages 10
 Number of subcatchments ... 5
 Number of nodes 2
 Number of links 1
 Number of pollutants 0
 Number of land uses 0

Raingage Summary

Name	Data Source	Data Type	Recording Interval
Chicago_4h_100yr	Chicago_4h_100yr	VOLUME	5 min.
Chicago_4h_25yr	Chicago_4h_25yr	VOLUME	5 min.
Chicago_4h_2yr	Chicago_4h_2yr	VOLUME	5 min.
Chicago_4h_50yr	Chicago_4h_50yr	VOLUME	5 min.
Chicago_4h_5yr	Chicago_4h_5yr	VOLUME	5 min.
SCS_Type_II_46.8mm_2yr_24hr_Collingwood	SCS_Type_II_46.8mm_2yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_60.3mm_5yr_24hr_Collingwood	SCS_Type_II_60.3mm_5yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_80.5mm_25yr_24hr_Collingwood	SCS_Type_II_80.5mm_25yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_88.8mm_50yr_24hr_Collingwood	SCS_Type_II_88.8mm_50yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_97.1mm_100yr_24hr_Collingwood	SCS_Type_II_97.1mm_100yr_24hr_Collingwood	INTENSITY	6 min.

Subcatchment Summary

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
201	4.64	264.00	50.00	2.0000	SCS_Type_II_60.3mm_5yr_24hr_Collingwood	SU1
202	6.71	314.00	50.00	2.0000	SCS_Type_II_60.3mm_5yr_24hr_Collingwood	SU1
203	1.27	138.00	0.00	2.0000	SCS_Type_II_60.3mm_5yr_24hr_Collingwood	SU1
204	1.07	400.00	50.00	2.0000	SCS_Type_II_60.3mm_5yr_24hr_Collingwood	SU1
205	1.90	750.00	50.00	2.0000	SCS_Type_II_60.3mm_5yr_24hr_Collingwood	SU1

Node Summary

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
OF1	OUTFALL	0.00	0.00	0.0	
SU1	STORAGE	189.60	3.90	0.0	

Link Summary

Name	From Node	To Node	Type	Length	%Slope	Roughness
OL1	SU1	OF1	OUTLET			

Cross Section Summary

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 5 YEAR STORM EVENT

Analysis Options

Flow Units CMS

Process Models:

Rainfall/Runoff YES
 RDII NO
 Snowmelt NO
 Groundwater NO
 Flow Routing YES
 Ponding Allowed NO
 Water Quality NO
 Infiltration Method HORTON
 Flow Routing Method DYNWAVE
 Surcharge Method EXTRAN
 Starting Date 10/13/2025 00:00:00
 Ending Date 10/14/2025 00:00:00
 Antecedent Dry Days 0.0
 Report Time Step 00:01:00
 Wet Time Step 00:05:00
 Dry Time Step 00:05:00
 Routing Time Step 5.00 sec
 Variable Time Step YES
 Maximum Trials 8
 Number of Threads 1
 Head Tolerance 0.001524 m

*****	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*****	-----	-----
Total Precipitation	0.940	60.300
Evaporation Loss	0.000	0.000
Infiltration Loss	0.338	21.673
Surface Runoff	0.593	38.026
Final Storage	0.011	0.693
Continuity Error (%)	-0.152	

*****	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.593	5.928
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	0.175	1.746
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.183	1.834
Final Stored Volume	0.602	6.015
Continuity Error (%)	0.006	

Time-Step Critical Elements

None

Highest Flow Instability Indexes

All links are stable.

Most Frequent Nonconverging Nodes

Convergence obtained at all time steps.

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 5 YEAR STORM EVENT

Routing Time Step Summary

```

Minimum Time Step      :    4.50 sec
Average Time Step      :    5.00 sec
Maximum Time Step      :    5.00 sec
% of Time in Steady State :    0.00
Average Iterations per Step :    2.00
% of Steps Not Converging :    0.00
Time Step Frequencies :
    5.000 - 3.155 sec :   100.00 %
    3.155 - 1.991 sec :    0.00 %
    1.991 - 1.256 sec :    0.00 %
    1.256 - 0.792 sec :    0.00 %
    0.792 - 0.500 sec :    0.00 %
  
```

Subcatchment Runoff Summary

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10 ⁶ ltr	Peak Runoff CMS	Runoff Coeff
201	60.30	0.00	0.00	20.04	30.07	9.59	39.66	1.84	0.55	0.658
202	60.30	0.00	0.00	20.04	30.05	9.52	39.57	2.65	0.77	0.656
203	60.30	0.00	0.00	40.08	0.00	19.14	19.14	0.24	0.04	0.317
204	60.30	0.00	0.00	20.04	30.13	9.94	40.07	0.43	0.15	0.665
205	60.30	0.00	0.00	20.04	30.13	9.95	40.08	0.76	0.27	0.665

Node Depth Summary

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
OF1	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
SU1	STORAGE	1.53	2.01	191.61	0 19:03	2.01

Node Inflow Summary

Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10 ⁶ ltr	Total Inflow Volume 10 ⁶ ltr	Flow Balance Error Percent
OF1	OUTFALL	0.000	0.033	0 19:03	0	1.75	0.000
SU1	STORAGE	1.778	1.778	0 11:54	5.93	7.76	0.006

Node Surcharge Summary

No nodes were surcharged.

Node Flooding Summary

No nodes were flooded.

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 5 YEAR STORM EVENT

Storage Volume Summary

Storage Unit	Average Volume 1000 m³	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m³	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CMS
SU1	4.050	22.3	0.0	0.0	6.138	33.8	0 19:03	0.033

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr
OF1	98.99	0.020	0.033	1.746
System	98.99	0.020	0.033	1.746

Link Flow Summary

Link	Type	Maximum Flow CMS	Time of Max Occurrence days hr:min	Maximum Veloc m/sec	Max/ Full Flow	Max/ Full Depth
OL1	DUMMY	0.033	0 19:03			

Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class							
		Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Tue Oct 14 20:45:07 2025
Analysis ended on: Tue Oct 14 20:45:07 2025
Total elapsed time: < 1 sec

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 25 YEAR STORM EVENT

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.2 (Build 5.2.4)

Element Count

Number of rain gages 10
 Number of subcatchments ... 5
 Number of nodes 2
 Number of links 1
 Number of pollutants 0
 Number of land uses 0

Raingage Summary

Name	Data Source	Data Type	Recording Interval
Chicago_4h_100yr	Chicago_4h_100yr	VOLUME	5 min.
Chicago_4h_25yr	Chicago_4h_25yr	VOLUME	5 min.
Chicago_4h_2yr	Chicago_4h_2yr	VOLUME	5 min.
Chicago_4h_50yr	Chicago_4h_50yr	VOLUME	5 min.
Chicago_4h_5yr	Chicago_4h_5yr	VOLUME	5 min.
SCS_Type_II_46.8mm_2yr_24hr_Collingwood	SCS_Type_II_46.8mm_2yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_60.3mm_5yr_24hr_Collingwood	SCS_Type_II_60.3mm_5yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_80.5mm_25yr_24hr_Collingwood	SCS_Type_II_80.5mm_25yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_88.8mm_50yr_24hr_Collingwood	SCS_Type_II_88.8mm_50yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_97.1mm_100yr_24hr_Collingwood	SCS_Type_II_97.1mm_100yr_24hr_Collingwood	INTENSITY	6 min.

Subcatchment Summary

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
201	4.64	264.00	50.00	2.0000	SCS_Type_II_80.5mm_25yr_24hr_Collingwood	SU1
202	6.71	314.00	50.00	2.0000	SCS_Type_II_80.5mm_25yr_24hr_Collingwood	SU1
203	1.27	138.00	0.00	2.0000	SCS_Type_II_80.5mm_25yr_24hr_Collingwood	SU1
204	1.07	400.00	50.00	2.0000	SCS_Type_II_80.5mm_25yr_24hr_Collingwood	SU1
205	1.90	750.00	50.00	2.0000	SCS_Type_II_80.5mm_25yr_24hr_Collingwood	SU1

Node Summary

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
OF1	OUTFALL	0.00	0.00	0.0	
SU1	STORAGE	189.60	3.90	0.0	

Link Summary

Name	From Node	To Node	Type	Length	%Slope	Roughness
OL1	SU1	OF1	OUTLET			

Cross Section Summary

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 25 YEAR STORM EVENT

Analysis Options

Flow Units CMS

Process Models:

Rainfall/Runoff YES
 RDII NO
 Snowmelt NO
 Groundwater NO
 Flow Routing YES
 Ponding Allowed NO
 Water Quality NO
 Infiltration Method HORTON
 Flow Routing Method DYNWAVE
 Surcharge Method EXTRAN
 Starting Date 10/13/2025 00:00:00
 Ending Date 10/14/2025 00:00:00
 Antecedent Dry Days 0.0
 Report Time Step 00:01:00
 Wet Time Step 00:05:00
 Dry Time Step 00:05:00
 Routing Time Step 5.00 sec
 Variable Time Step YES
 Maximum Trials 8
 Number of Threads 1
 Head Tolerance 0.001524 m

*****	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*****	-----	-----
Total Precipitation	1.255	80.500
Evaporation Loss	0.000	0.000
Infiltration Loss	0.406	26.011
Surface Runoff	0.838	53.754
Final Storage	0.013	0.864
Continuity Error (%)	-0.159	

*****	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	0.838	8.380
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	0.209	2.091
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.183	1.834
Final Stored Volume	0.812	8.122
Continuity Error (%)	0.007	

Time-Step Critical Elements

None

Highest Flow Instability Indexes

All links are stable.

Most Frequent Nonconverging Nodes

Convergence obtained at all time steps.

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 25 YEAR STORM EVENT

Routing Time Step Summary

```

Minimum Time Step      :    4.50 sec
Average Time Step      :    5.00 sec
Maximum Time Step      :    5.00 sec
% of Time in Steady State :    0.00
Average Iterations per Step :    2.00
% of Steps Not Converging :    0.00
Time Step Frequencies :
    5.000 - 3.155 sec :   100.00 %
    3.155 - 1.991 sec :    0.00 %
    1.991 - 1.256 sec :    0.00 %
    1.256 - 0.792 sec :    0.00 %
    0.792 - 0.500 sec :    0.00 %
  
```

Subcatchment Runoff Summary

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10 ⁶ ltr	Peak Runoff CMS	Runoff Coeff
201	80.50	0.00	0.00	24.05	40.18	15.54	55.71	2.59	0.78	0.692
202	80.50	0.00	0.00	24.05	40.15	15.45	55.60	3.73	1.10	0.691
203	80.50	0.00	0.00	48.10	0.00	31.04	31.04	0.39	0.07	0.386
204	80.50	0.00	0.00	24.05	40.23	16.00	56.23	0.60	0.22	0.698
205	80.50	0.00	0.00	24.05	40.23	16.01	56.23	1.07	0.39	0.699

Node Depth Summary

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
OF1	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
SU1	STORAGE	1.73	2.40	192.00	0 20:06	2.40

Node Inflow Summary

Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10 ⁶ ltr	Total Inflow Volume 10 ⁶ ltr	Flow Balance Error Percent
OF1	OUTFALL	0.000	0.040	0 20:06	0	2.09	0.000
SU1	STORAGE	2.544	2.544	0 11:54	8.38	10.2	0.007

Node Surcharge Summary

No nodes were surcharged.

Node Flooding Summary

No nodes were flooded.

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 25 YEAR STORM EVENT

Storage Volume Summary

Storage Unit	Average Volume 1000 m³	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m³	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CMS
SU1	5.081	27.9	0.0	0.0	8.186	45.0	0 20:06	0.040

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr
OF1	99.19	0.024	0.040	2.091
System	99.19	0.024	0.040	2.091

Link Flow Summary

Link	Type	Maximum Flow CMS	Time of Max Occurrence days hr:min	Maximum Veloc m/sec	Max/ Full Flow	Max/ Full Depth
OL1	DUMMY	0.040	0 20:06			

Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class								
		Up Dry	Down Dry	Sub Dry	Sup Crit	Up Crit	Down Crit	Norm Crit	Inlet Ltd	Ctrl

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Tue Oct 14 20:45:43 2025
Analysis ended on: Tue Oct 14 20:45:43 2025
Total elapsed time: < 1 sec

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 100 YEAR STORM EVENT

EPA STORM WATER MANAGEMENT MODEL - VERSION 5.2 (Build 5.2.4)

Element Count

Number of rain gages 10
 Number of subcatchments ... 5
 Number of nodes 2
 Number of links 1
 Number of pollutants 0
 Number of land uses 0

Raingage Summary

Name	Data Source	Data Type	Recording Interval
Chicago_4h_100yr	Chicago_4h_100yr	VOLUME	5 min.
Chicago_4h_25yr	Chicago_4h_25yr	VOLUME	5 min.
Chicago_4h_2yr	Chicago_4h_2yr	VOLUME	5 min.
Chicago_4h_50yr	Chicago_4h_50yr	VOLUME	5 min.
Chicago_4h_5yr	Chicago_4h_5yr	VOLUME	5 min.
SCS_Type_II_46.8mm_2yr_24hr_Collingwood	SCS_Type_II_46.8mm_2yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_60.3mm_5yr_24hr_Collingwood	SCS_Type_II_60.3mm_5yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_80.5mm_25yr_24hr_Collingwood	SCS_Type_II_80.5mm_25yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_88.8mm_50yr_24hr_Collingwood	SCS_Type_II_88.8mm_50yr_24hr_Collingwood	INTENSITY	6 min.
SCS_Type_II_97.1mm_100yr_24hr_Collingwood	SCS_Type_II_97.1mm_100yr_24hr_Collingwood	INTENSITY	6 min.

Subcatchment Summary

Name	Area	Width	%Imperv	%Slope	Rain Gage	Outlet
201	4.64	264.00	50.00	2.0000	SCS_Type_II_97.1mm_100yr_24hr_Collingwood	SU1
202	6.71	314.00	50.00	2.0000	SCS_Type_II_97.1mm_100yr_24hr_Collingwood	SU1
203	1.27	138.00	0.00	2.0000	SCS_Type_II_97.1mm_100yr_24hr_Collingwood	SU1
204	1.07	400.00	50.00	2.0000	SCS_Type_II_97.1mm_100yr_24hr_Collingwood	SU1
205	1.90	750.00	50.00	2.0000	SCS_Type_II_97.1mm_100yr_24hr_Collingwood	SU1

Node Summary

Name	Type	Invert Elev.	Max. Depth	Ponded Area	External Inflow
OF1	OUTFALL	0.00	0.00	0.0	
SU1	STORAGE	189.60	3.90	0.0	

Link Summary

Name	From Node	To Node	Type	Length	%Slope	Roughness
OL1	SU1	OF1	OUTLET			

Cross Section Summary

Conduit	Shape	Full Depth	Full Area	Hyd. Rad.	Max. Width	No. of Barrels	Full Flow

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 100 YEAR STORM EVENT

Analysis Options

Flow Units CMS

Process Models:

Rainfall/Runoff YES
 RDII NO
 Snowmelt NO
 Groundwater NO
 Flow Routing YES
 Ponding Allowed NO
 Water Quality NO
 Infiltration Method HORTON
 Flow Routing Method DYNWAVE
 Surcharge Method EXTRAN
 Starting Date 10/13/2025 00:00:00
 Ending Date 10/14/2025 00:00:00
 Antecedent Dry Days 0.0
 Report Time Step 00:01:00
 Wet Time Step 00:05:00
 Dry Time Step 00:05:00
 Routing Time Step 5.00 sec
 Variable Time Step YES
 Maximum Trials 8
 Number of Threads 1
 Head Tolerance 0.001524 m

*****	Volume	Depth
Runoff Quantity Continuity	hectare-m	mm
*****	-----	-----
Total Precipitation	1.514	97.100
Evaporation Loss	0.000	0.000
Infiltration Loss	0.452	28.971
Surface Runoff	1.049	67.295
Final Storage	0.015	0.993
Continuity Error (%)	-0.164	

*****	Volume	Volume
Flow Routing Continuity	hectare-m	10^6 ltr
*****	-----	-----
Dry Weather Inflow	0.000	0.000
Wet Weather Inflow	1.049	10.491
Groundwater Inflow	0.000	0.000
RDII Inflow	0.000	0.000
External Inflow	0.000	0.000
External Outflow	0.245	2.450
Flooding Loss	0.000	0.000
Evaporation Loss	0.000	0.000
Exfiltration Loss	0.000	0.000
Initial Stored Volume	0.183	1.834
Final Stored Volume	0.987	9.874
Continuity Error (%)	0.007	

Time-Step Critical Elements

None

Highest Flow Instability Indexes

All links are stable.

Most Frequent Nonconverging Nodes

Convergence obtained at all time steps.

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 100 YEAR STORM EVENT

Routing Time Step Summary

```

Minimum Time Step      :    4.50 sec
Average Time Step      :    5.00 sec
Maximum Time Step      :    5.00 sec
% of Time in Steady State :    0.00
Average Iterations per Step :    2.00
% of Steps Not Converging :    0.00
Time Step Frequencies :
    5.000 - 3.155 sec :   100.00 %
    3.155 - 1.991 sec :    0.00 %
    1.991 - 1.256 sec :    0.00 %
    1.256 - 0.792 sec :    0.00 %
    0.792 - 0.500 sec :    0.00 %
  
```

Subcatchment Runoff Summary

Subcatchment	Total Precip mm	Total Runon mm	Total Evap mm	Total Infil mm	Imperv Runoff mm	Perv Runoff mm	Total Runoff mm	Total Runoff 10 ⁶ ltr	Peak Runoff CMS	Runoff Coeff
201	97.10	0.00	0.00	26.79	48.48	21.00	69.48	3.22	0.98	0.716
202	97.10	0.00	0.00	26.79	48.45	20.90	69.35	4.65	1.38	0.714
203	97.10	0.00	0.00	53.58	0.00	41.95	41.95	0.53	0.11	0.432
204	97.10	0.00	0.00	26.79	48.52	21.55	70.07	0.75	0.28	0.722
205	97.10	0.00	0.00	26.79	48.52	21.55	70.08	1.33	0.50	0.722

Node Depth Summary

Node	Type	Average Depth Meters	Maximum Depth Meters	Maximum HGL Meters	Time of Max Occurrence days hr:min	Reported Max Depth Meters
OF1	OUTFALL	0.00	0.00	0.00	0 00:00	0.00
SU1	STORAGE	1.89	2.70	192.30	0 18:56	2.70

Node Inflow Summary

Node	Type	Maximum Lateral Inflow CMS	Maximum Total Inflow CMS	Time of Max Occurrence days hr:min	Lateral Inflow Volume 10 ⁶ ltr	Total Inflow Volume 10 ⁶ ltr	Flow Balance Error Percent
OF1	OUTFALL	0.000	0.059	0 18:56	0	2.45	0.000
SU1	STORAGE	3.222	3.222	0 11:54	10.5	12.3	0.007

Node Surcharge Summary

No nodes were surcharged.

Node Flooding Summary

No nodes were flooded.

DEY DRIVE TOWNHOUSES – SWM MODELLING – SCS 100 YEAR STORM EVENT

Storage Volume Summary

Storage Unit	Average Volume 1000 m³	Avg Pcnt Full	Evap Pcnt Loss	Exfil Pcnt Loss	Maximum Volume 1000 m³	Max Pcnt Full	Time of Max Occurrence days hr:min	Maximum Outflow CMS
SU1	5.965	32.8	0.0	0.0	9.916	54.6	0 18:56	0.059

Outfall Loading Summary

Outfall Node	Flow Freq Pcnt	Avg Flow CMS	Max Flow CMS	Total Volume 10^6 ltr
OF1	99.30	0.029	0.059	2.450
System	99.30	0.029	0.059	2.450

Link Flow Summary

Link	Type	Maximum Flow CMS	Time of Max Occurrence days hr:min	Maximum Veloc m/sec	Max/ Full Flow	Max/ Full Depth
OL1	DUMMY	0.059	0 18:56			

Flow Classification Summary

Conduit	Adjusted /Actual Length	Fraction of Time in Flow Class							
		Up Dry	Down Dry	Sub Crit	Sup Crit	Up Crit	Down Crit	Norm Ltd	Inlet Ctrl

Conduit Surcharge Summary

No conduits were surcharged.

Analysis begun on: Tue Oct 14 20:46:11 2025
Analysis ended on: Tue Oct 14 20:46:11 2025
Total elapsed time: < 1 sec

Appendix D

BACKGROUND INFORMATION

FUNCTIONAL SERVICING REPORT

**DEY DRIVE TOWNHOUSES
TOWN OF COLLINGWOOD**

From: [Dan Hurley](#)
To: [Travis Burnside](#)
Cc: [John Welton](#); [Michael Uster](#)
Subject: RE: Pretty River Estates.
Date: November 13, 2020 9:01:59 AM
Attachments: [image001.png](#)
[image002.png](#)
[image003.png](#)
[image004.png](#)
[L - NVCA - Response to Draft Plan of Subdivision Comments.pdf](#)
[L - NVCA - Response to Parcel 1 and 2 Hydraulic Comments.pdf](#)

Hello Travis – received your message thanks.

We were not the engineers for Liberty for Phase 1 of their development. We became involved to sort out floodplain issues associated with Parcels 1 and 2 so the information we have is more focused on the floodplain related matters. That being said.

- I do have some excerpts from a Preliminary SWM Report prepared for the Phase 2 lands that was authored by Exp in 2011. I can send what I have do not have the full copy – might be best to get that from Michael.
- Yes both Parcels 1 and 2 will need to be flood protected to above 194.5 with lowest openings for any dwelling above 194.8. Also for Parcel 2 there is the matter of the small spill from the river that is currently conveyed along the parcels very east limit. This will need to be addressed in the design of Parcel 2 and our letters attached describe 2 ways this can be addressed. The Town/NVCA would have to be consulted to confirm which approach is preferred through the design process.
- I do not have the history with regard to the easement width – sorry.

Hope this helps

Dan Hurley, B.A.Sc., P.Eng., LEED AP
President

Tatham Engineering Limited
115 Sandford Fleming Drive, Suite 200 | Collingwood | Ontario | L9Y 5A6
T 705-444-2565 x2040 | C 705-444-7571 | dhurley@tathameng.com | tathameng.com



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From: Travis Burnside <tburnside@cobideeng.com>
Sent: November 12, 2020 1:43 PM
To: Dan Hurley <dhurley@tathameng.com>
Cc: John Welton <johnzwelton@sunvalehomes.com>
Subject: RE: Pretty River Estates.

Dan

I left you a voicemail and thought I would follow up with an email.

Are you able to provide the following information:

- Pretty River Estates SWM Report
- Regional Flood Elevation that Parcel 1 must stay above? My understanding based on the information provided to John for Parcel 2 is that the south limit of Parcel 2 is be built up to an

elevation of 194.50 m.

- Do you know if there is a reason why the sewer easement though Parcel 1 widens out on an angle when the sewers run straight across the site? Can the easement be modified to allow that land to be used for building purposes?

Thank You

Travis

Travis Burnside, P. Eng.

Cobide Engineering Inc.

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Hanover, ON N4N 1R4

T +1 519-506-5959 #101

C +1 519-901-5959

E tburnside@cobideeng.com

www.cobideeng.com

From: John Welton <johnzwelton@sunvalehomes.com>

Sent: November 12, 2020 12:43 PM

To: Travis Burnside <tburnside@cobideeng.com>

Subject: FW: Pretty River Estates.

From: Dan Hurley <dhurley@tathameng.com>

Sent: October 30, 2020 8:29 AM

To: John Welton <johnzwelton@sunvalehomes.com>

Subject: RE: Pretty River Estates.

Hello John – following up on these parcels to see if you were still proceeding. Happy to assist where and when necessary.

Thanks – hope all is well.

Regards,

Dan Hurley, B.A.Sc., P.Eng., LEED AP

President

Tatham Engineering Limited

115 Sandford Fleming Drive, Suite 200 | Collingwood | Ontario | L9Y 5A6

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File 117003

May 16, 2019

'WITHOUT PREJUDICE'

Amy Knapp
Planner II
Nottawasaga Valley Conservation Authority
8195 8th Line
Utopia, Ontario L0M 1T0
aknapp@nvca.on.ca

Re: Proposed Draft Plan of Condominium and Part Lot Control
Proposed Official Plan Amendment and Zoning By-law Amendment
Phase II of Pretty River Estates, Liberty Draft Plan of Subdivision
Town of Collingwood, Part Lot 40, Concession 8
Town of Collingwood - File No. CW-T-0101
NVCA ID # 19723

Dear Amy:

This letter has been prepared in response to the NVCA comments letter dated March 25, 2019 regarding the above noted project. Specifically, it will address the engineering questions contained therein in the order they were presented as follows.

ENGINEERING

1. *NVCA staff accept the findings of the flood study and erosion hazard delineation for the site.*
Noted.
2. *In order to finalize the limits of development and lot configuration we will require the following information:*
 - a. *An updated lot fabric showing all parcels are located outside of the 100-year flood extents, erosion hazard (including 6 metre access allowance), and spill area extents.*

Specific to the limits of development we have attached the line work showing the limit of Parcels 1 and 2 and can confirm they respect the identified setbacks (see Figure 1.0 attached). Fill is proposed for the south-east corner of Parcel 2 and preliminary grades are illustrated that will eliminate the spill to the north and ensure it will flow over the rail trail and back into the Pretty River main channel. The updated spill model is included with this submission. We have not shown the internal lot fabric for Parcel 1 and 2 as that is still being developed and will be subject to the site plan approval process along with detailed grading.

We note Parcel 3 is not included on this plan as development on this parcel is proposed to be deferred for the time being.

- b. *The status of the outcome of any further discussions with the Town on their requirements for a cumulative impact assessment and the potential for improving or eliminating the existing spill to the north.*

Tatham Engineering has consulted with the Town specific to cumulative impact and can confirm the following:

- The Town is not aware of any other applications proposing to develop in the flood fringe downstream of the PRE Phase 2 site.
- The PRE Phase 2 site is at the upstream limit of the special policy (2-Zone) area. Upstream is Township of Clearview and a 1-Zone policy area.
- The flood fringe downstream of the PRE Phase 2 site (downstream of the rail crossing) is small as there is no structure that causes the backwater condition experienced at the PRE Phase 2 site. In fact, the flood level difference between the 1:100 year and Regulatory flows is only +/- 0.3 – 0.5 m thus creating a small flood fringe with limited storage capacity.
- The Town confirmed they have reviewed and approved many development proposals in the flood spill downstream of the PRE Phase 2 site (as has the NVCA) and have never required or been requested to provide a cumulative impact assessment.

- c. *Preliminary lot grading plans demonstrating that safe access / egress and flood-proofing to and within all parcels as per NVCA criteria is achievable.*

Fill will be required to bring Parcels 1 and 2 above the Regulatory Storm Event flood elevations. Internal roads shall be graded above 194.20 m, which is the maximum Regulatory Storm Event flood elevation. The minimum opening elevation for all proposed dwellings shall be 194.50 m, which is at 0.30 m above the Regulatory Storm Event flood elevation for the entire development. The lot grading detail will be dealt with at the site plan stage.

Spill through Parcel 2 is proposed to be eliminated through the raising of the grade across the parcel and along the south limit of the property. Under the Regulatory Storm Event, there is still potential for spill to occur over the rail crossing up to an elevation of approximately 194.15 m. All Parcel 2 lots will be graded above the spill elevation as depicted on Figure 2.0.

As previously indicated, development on Parcel 3 is proposed to be deferred for now.

- d. *Preliminary stormwater management calculations and supporting information. In cases where a lot will drain to an existing pond, information that confirms the proposed drainage area characteristics are consistent with the original pond design are sufficient. However, it is noted that the Eden Oak SWM pond design did not consider external drainage from Parcel 2 and it would*



need to be demonstrated that this pond can accommodate the additional drainage area. The locations of any proposed outlets and emergency overland flow routes should also be indicated.

Stormwater management will be dealt with the site plan stage within the parcels identified on within the approved subdivision plans (PRE Phase 1 or Eden Oak).

We trust that this response addresses the outstanding engineering concerns as it relates to the proposal to amend the Town's Official plan and Zoning By-law in support of Phase II of the Pretty River Estates.

Yours truly,

Tatham Engineering Limited



Dan Hurley B.A.Sc., P.Eng., LEED AP
President
DJH/DAM:rlh



David Marshall B.A.Sc., P.Eng.
Intermediate Engineer

copy:	Peter Alm	NVCA	email (palm@nvca.on.ca)
	Mark Bryan	Town of Collingwood	email (mbryan@collingwood.ca)
	John Velick	Town of Collingwood	email (jvelick@collingwood.ca)
	Mark Liddy	Liberty Development	email (mark@libertydevelopment.ca)

I:\2017 Projects\117003 - Pretty River Hydrology Review\Documents\L - NVCA - Response to Draft Plan of Subdivision Comments.docx



Figure 1



Figure 2



CONDELAND ENGINEERING LIMITED
TECHNICAL DIVISION
STORM WATER MANAGEMENT ANALYSIS

PROJECT NUMBER: 15-010

PROJECT LOCATION: PROPOSED RESIDENTIAL DEVELOPMENT
EAST OF HURONTARIO STREET NORTH OF POPLAR
Town of Collingwood

CLIENT: EDEN OAK (MC NABB) INC.

East SWM Pond Characteristics
Stage-Storage-Discharge Relationship

orifice invert = 191.9
orifice dia = 0.5
orifice centroid ele. = 192.15
weir length = 3
weir elevation 193
orifice area = 0.19625
ICD invert = 190.6

ELEVATION (m)	DEPTH (m)	AREA (sq.m.)	STORAGE (cu.m.)	STORAGE (Ha-m)	ICD Type 'C' Discharge Rate (lps)			ICD Type 'C' Discharge Rate (cum/sec)	Head on orifice (m)	Orifice Discharge (invert 190.70 in cum/sec)	Weir Discharge	Total Discharge (cum/sec)
189.60	0.00	1080.56	0.00	0.0000		FOREBAY						
189.90	0.30	1266.73	123.77	0.0124	0.00		0.0000	0.00	0.00	0.00	0.0000	
190.00	0.40	1333.95	312.66	0.0313	0.00		0.0000	0.00	0.00	0.00	0.0000	
190.20	0.60	1471.19	370.17	0.0370	0.00		0.0000	0.00	0.00	0.00	0.0000	
190.30	0.70	1541.20	801.25	0.0801	0.00		0.0000	0.00	0.00	0.00	0.0000	
190.40	0.80	3240.68	966.26	0.0966	0.00	PERMANENT POOL	0.0000	0.00	0.00	0.00	0.0000	
190.50	0.90	3420.18	1459.47	0.1459	0.00		0.0000	0.00	0.00	0.00	0.0000	
190.60	1.00	3551.17	1808.04	0.1808	0.00		0.0000	0.00	0.00	0.00	0.0000	
190.70	0.80	3741.96	367.91	0.0368	11.00		0.0000	0.00	0.00	0.00	0.0000	
190.80	0.90	2876.50	748.83	0.0749	16.00		0.0110	0.00	0.0000	0.0000	0.0110	0.0000
190.90	1.00	4019.66	1143.64	0.1144	19.00	ACTIVE STORAGE	0.0160	0.00	0.0000	0.0000	0.0160	0.0368
191.00	1.10	4144.23	1551.83	0.1552	22.00		0.0190	0.00	0.0000	0.0000	0.0190	0.0749
191.10	1.20	4270.48	1972.57	0.1973	24.50		0.0220	0.00	0.0000	0.0000	0.0220	0.1144
191.20	1.30	4398.41	2406.01	0.2406	26.50		0.0245	0.00	0.0000	0.0000	0.0245	0.1552
191.30	1.40	4528.01	2852.33	0.2852	28.50		0.0265	0.00	0.0000	0.0000	0.0265	0.1973
191.40	1.50	4659.30	3311.7	0.3312	30.00		0.0285	0.00	0.0000	0.0000	0.0285	0.2406
191.50	1.60	4792.26	3784.28	0.3784	31.50		0.0300	0.00	0.0000	0.0000	0.0300	0.2852
191.60	1.70	4926.89	4270.24	0.4270	33.00		0.0315	0.00	0.0000	0.0000	0.0315	0.3312
191.70	1.80	5063.21	4769.74	0.4770	34.50		0.0330	0.00	0.0000	0.0000	0.0330	0.3784
191.80	1.90	5201.20	5282.96	0.5283	36.50		0.0345	0.00	0.0000	0.0000	0.0345	0.4270
191.90	2.00	5340.87	5810.06	0.5810	38.00		0.0365	0.00	0.0000	0.0000	0.0365	0.4770
192.00	2.10	5482.22	6351.22	0.6351	39.50		0.0380	0.00	0.0000	0.0000	0.0380	0.5283
192.10	2.20	5626.49	6906.65	0.6907	41.00		0.0395	0.00	0.0000	0.0000	0.0395	0.5810
192.20	2.30	5773.00	7476.64	0.7477	42.50		0.0410	0.00	0.0000	0.0000	0.0410	0.6351
192.30	2.40	5922.29	8061.42	0.8061	44.00		0.0425	0.00	0.0000	0.0000	0.0425	0.6907
192.40	2.50	6073.48	8661.21	0.8661	45.50		0.0440	0.00	0.0000	0.0000	0.0440	0.7477
192.50	2.60	6226.85	9276.23	0.9276	47.00		0.0455	0.25	0.3564	0.0000	0.4019	0.8061
192.60	2.70	6382.42	9906.69	0.9907	47.33		0.0470	0.35	0.4217	0.0000	0.4687	0.8661
192.70	2.80	6541.59	10552.89	1.0553	47.67		0.0473	0.45	0.4782	0.0000	0.5255	0.9276
192.80	2.90	6705.95	11215.27	1.1215	48.00		0.0477	0.55	0.5286	0.0000	0.5763	0.9907
192.90	3.00	6874.60	11894.3	1.1894	48.33		0.0480	0.65	0.5747	0.0000	0.6227	1.0553
193.00	3.10	7047.55	12590.4	1.2590	48.67		0.0483	0.75	0.6173	0.0000	0.6656	1.1215
193.10	3.20	7248.97	13305.23	1.3305	49.00		0.0487	0.85	0.6572	0.0000	0.7058	1.1894
193.20	3.30	7429.63	14039.16	1.4039	49.33		0.0490	0.95	0.6948	0.0000	0.7500	1.2590
193.30	3.40	7592.43	14790.26	1.4790	49.67		0.0493	1.05	0.7304	0.4562	1.2359	1.3305
193.40	3.50	7781.22	15558.95	1.5559	50.00		0.0497	1.15	0.7644	0.8380	1.6521	1.4039
193.50	3.60	7975.04	16346.76	1.6347	50.33		0.0500	1.25	0.7969	1.2902	2.1372	1.4790
							0.0503	1.35	0.8282	1.8031	2.6817	1.5559
												1.6347