

# **MEDIBUDZ COLLINGWOOD**

**Town of Collingwood** 

**Functional Servicing Report** 

prepared by:

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Medibudz Canada Ltd.

August 9, 2018 Revised October 1, 2018

CCTA File 118076

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#### Introduction 1

C.C. Tatham & Associates Ltd. (CCTA) has been retained by Medibudz Canada Ltd. to prepare a Functional Servicing Report in support of the proposed medical cannabis indoor production facility at 135 Sandford Fleming Drive in the Town of Collingwood, County of Simcoe. This report has been prepared to address the internal and external servicing requirements associated with this project. Specifically, this report will address the stormwater management, potable water supply, sanitary sewage collection and conveyance and utility distribution for the proposed development.

#### 1.1 Site Description

The proposed development site has an area of 1.93 ha with approximately 61 m of frontage on Sandford Fleming Drive. Legally described as Part 3 of Lot 41, Concession 7 and zoned M5 – Industrial Park, the property is currently vacant and mainly comprised of gravel and small to medium rocks with some vegetation on the east side.

The property is bounded by Habitat for Humanity ReStore to the north, C.C. Tatham & Associates Ltd., CrossFit Mozomo and Head Over Heels Gymnastics Club to the south, Pilkington Glass of Canada to the east and Sandford Fleming Drive to the west. Figure 1.0 – Site Location Plan is enclosed for reference.

A topographic survey of the property was completed by C.C. Tatham & Associates Ltd. in June, 2018. The topography of the site was observed to slope from south to north towards a drainage channel that runs along the north property line and conveys stormwater to an existing stormwater management (SWM) pond north of the site. Additional drainage channels along the south, west and east property boundaries convey stormwater around the site to the aforementioned SWM pond.

#### 1.2 **Geotechnical Investigation**

Geotechnical investigations were completed by Cambium Inc. at the subject property in July, 2018 to assess the subsurface conditions. The field work consisted of 8 boreholes extended to a termination depth of 1.9 meters below ground surface (mbgs) to 5.2 mbgs at various locations across the site.

All boreholes encountered a surficial layer of imported fill ranging in depth between 0.6 mbgs to 2.4 mbgs. The fill generally consisted of brown gravelly sand to sand with gravel. Underlying the layer of fill was native soils consisting of glaciolacustrine deposits generally consisting of sand overlying sand and gravel to the termination depths of 1.9 mbgs to 5.1 mbgs. The native soils were predominantly brown to grey sand with some silt and trace to some gravel overlying grey sand and gravel with some silt. Bedrock was not encountered during the investigation. Upon completion of drilling and prior to backfill, groundwater was encountered in seven of the boreholes while caving (sloughing) was encountered in six of the boreholes.

The geotechnical report includes recommendations for the construction of the proposed building, driveway and parking area and earthworks. There do not appear to be any significant geotechnical concerns which would adversely impact the proposed development. The geotechnical report will be provided under separate cover.

### 1.3 Proposed Land Use

The proposed development will include the construction of a 4,645 sq.m (50,000 sq.ft) medical marijuana grow operation facility. The remainder of the site will consist of an asphalt and gravel parking lot and vacant land slated for future expansion.





MEDIBUDZ COLLINGWOOD LTD. 135 SANFORD FLEMING DR. SITE LOCATION PLAN

DWG. No.

FIG. 1

SCALE: NTS DATE: JULY 2018

JOB NO. 118076

## 2 Servicing Requirements

Municipal servicing is located on the west side of Sandford Fleming Drive in the form of a 300 mm diameter DI watermain and a 300 mm diameter PVC sanitary sewer. An existing 150 mm diameter PVC sanitary service at a slope of approximately 3.5% and a 50 mm diameter copper water service extend to the property line along Sandford Fleming Drive. The location of the sanitary sewer and watermain along with existing services was confirmed by reviewing As-Built drawings of Sandford Fleming Drive provided by the Town of Collingwood. The Site Servicing Plan (SS-1) has been appended to this report for reference.

### 2.1 Sanitary Sewer Servicing

A detailed analysis of the expected sanitary flows to be generated by the development was prepared by HL Engineering Ltd. (Appendix A) and is summarized as follows:

Peak Flow: 3.9 L/s

Daily Average: 5,750 L

Maximum Day: 11,730 L

Considering the potential for future expansion, HL Engineering confirmed that the existing 150 mm diameter sanitary service will have adequate capacity to service the property.

### 2.2 Potable Water Servicing

A detailed analysis of the expected potable water requirements for the development was prepared by HL Engineering Ltd. (Appendix A) and is summarized as follows:

Peak Flow: 5.3 L/s

Daily Average: 6,510 L

Maximum Day: 11,580 L

Fire Demand: 54 L/s

Considering the potential for future expansion, HL Engineering recommended that a 100 mm diameter water service be installed to provide the expected 5.3 L/s of domestic and process water for the site. A separate 150 mm diameter fire service was also recommended to provide the required fire protection. A

single 150 mm diameter water service will be extended to the property line where it will be split into the separate fire and domestic services internal to the property.

It is expected that the 300 mm diameter watermain will have adequate flow and pressure to service the property, however, the proposed water system will need to be added to the Town's overall water model to ensure the demands can be provided.

An existing fire hydrant is located on the west side of the cul-de-sac, approximately 75 m from the proposed indoor production facility. An additional fire hydrant is proposed to be located internal to the site, adjacent to the proposed Medibudz entrance, approximately 45 m from the existing hydrant. The proposed hydrant location is shown on the Site Servicing Plan (SS-1) attached.

## 3 Stormwater Management

The stormwater management (SWM) strategy for the proposed development site was prepared recognizing the pertinent Conservation Authority, Municipal and Provincial guidelines on water resources including the following:

- Stormwater Management Planning and Design Manual, Ministry of the Environment (March 2003);
- Collingwood East End Drainage Study, C.C. Tatham & Associates Ltd. (March 2014);
- NVCA Stormwater Technical Guide, Nottawasaga Valley Conservation Authority (December 2013);
   and
- Development Standards, Corporation of the Town of Collingwood (July 2007).

### 3.1 Stormwater Management Criteria

Several environmental factors and site conditions govern the design of the stormwater management plan for the development. In keeping with the recommendations provided in the East End Study, the SWM criteria to be adhered to are as follows:

- safely convey all storms up to and including the regional storm event to the existing SWM pond; and
- promote groundwater recharge and infiltration where possible.

The site is located within a portion of the Sandford Fleming Industrial Park (Catchment 200 of Fig. 2, attached) which has existing drainage infrastructure in the form of ditches that surround the site and convey runoff to an existing SWM pond north east of the Habitat for Humanity ReStore. The eventual downstream outlet to Georgian Bay along Elliott Avenue has also been upgraded to support the flows from Catchment 200. The proposed Medibudz site is consistent with the Overall Drainage Plan (Fig. 2) and will continue to direct runoff to the existing drainage infrastructure, ultimately discharging to the existing SWM pond.

### 3.1.1 Proposed Conditions

Under existing conditions, the overall percent impervious for the 13.7 ha industrial subdivision was calculated to be 40%. Under proposed conditions, the overall percent impervious increases to 47%. This is in general conformance with the overall percent impervious of 45% which was utilized in completing the industrial subdivision SWM pond improvement calculations (see attached), completed as part of the Collingwood East End Drainage Study (March 2014). Thus, the existing SWM pond was sized assuming the Medibudz site would eventually be developed.

The runoff from the Medibudz site along with parts of the adjacent properties to the side yard ditches along the property lines was calculated for the proposed condition. The estimated 100-yr peak runoff rate was calculated using the Modified Rational Equation and the capacity of the ditches at the specified cross-sections was determined utilizing the Manning's Equation for channel flow. All calculations have been attached for reference. It was determined that the existing ditches will have adequate capacity to convey the 100-year flows to the existing SWM pond. The results have been summarized below:

### North Ditch

Approximate drainage area from parts of Medibudz and Habitat ReStore: 0.78 ha

Estimated runoff coefficient: 0.63

Estimated 100-year Peak Runoff Rate: 0.277 cms

Section A-A Flow Capacity: 0.81 cms

Section B-B Flow Capacity: 2.78 cms

Section F-F Flow Capacity: 1.22 cms

### South Ditch

Approximate drainage area from parts of Medibudz and Habitat ReStore: 2.25 ha

Estimated runoff coefficient: 0.60

Estimated 100-year Peak Runoff Rate: 0.761 cms

Section C-C Flow Capacity: 3.39 cms

Section D-D Flow Capacity: 6.60 cms

Section G-G Flow Capacity: 1.56 cms

The proposed 27.6 m 600 mm diameter driveway culvert will convey flow from the roadside ditch across the Medibudz and Habitat for Humanity driveways and will discharge into the roadside ditch just upstream of the existing 6.0 m 600 mm diameter driveway culvert.

The proposed culvert was sized to ensure the existing 6.0 m driveway culvert continues to provide control for the ditch. The existing culvert can convey 0.45 m³/s before the water overtops the road, and the proposed culvert will convey 0.65 m³/s prior to overtopping the road. Model results for both culverts have been provided in Appendix A and drawing DP-2 has been included for reference.

### 3.1.2 Existing SWM Pond Characteristics

In accordance with recommendations provided in the Collingwood East End Drainage Study (March 2014), the existing SWM pond was subjected to the following improvements to ensure the required quantity and quality treatment can be provided:

- a sediment forebay was constructed to facilitate sediment settling and provide an isolated area for future sediment removal;
- the bottom of the pond was excavated approximately 1.0 m deeper to increase the volume of storage provided;
- the primary outlet was removed and replaced with a perforated vertical riser outlet and low flow control
  pipe. The perforated vertical riser was encased in rip rap to filter sediment from the surface runoff
  prior to being discharged downstream;
- the low flow control outlet was sized to optimize the peak flow attenuation provided in the pond during minor storm events;
- the wetland cell was seeded with wetland plantings to improve sediment filtration and phosphorous uptake;
- the overflow spillway was removed and a proper overflow spillway was constructed to control the release of major storm peak flows downstream while preventing the pond banks for being overtopped; and
- the pond banks above the permanent pool water level were planted with upland and buffer vegetation to improve shading, lover pond water temperatures and create upland habitat around the perimeter of the pond.

The existing Stormwater Management Pond Improvements Plan (PND-1) has been attached for reference.

Based on the conclusions from the Collingwood East End Drainage Study (March 2014), it is expected that the existing SWM pond will accommodate the runoff from the Medibudz site.

### 3.1.3 Siltation and Erosion Controls

Siltation and erosion controls will be implemented for all construction activities, including topsoil stripping, material stockpiling and grading operations. The following sediment and erosion control measures are to be implemented during construction:

 heavy duty silt fence will be erected before the commencement of any grading operations to control sediment movement;

- a construction vehicle entrance will be constructed and maintained consisting of a stone mud mat to reduce off-site tracking of material;
- regular inspection of control measures will be instituted and repairs will be made as necessary; and
- temporary swales and check dams will be constructed to prevent transportation of sediment off-site or into the existing SWM pond.

The Siltation & Erosion Control Plan (SC-1) has been attached to this report for reference.

# 4 Utility Network

It has been acknowledged that the following utility providers have services along Sandford Fleming:

- Bell Canada;
- Rogers Cable;
- Collus Powerstream; and
- Enbridge Gas.

The specific servicing requirements will be established by formally submitting connection requests to each utility provider.

### 5 Conclusions and Recommendations

The proposed Functional Servicing Report demonstrates that the development has adequate services available to meet the established criteria with regards to general servicing and stormwater management and can proceed without negatively impacting the existing infrastructure.

Stormwater will be conveyed to the existing SWM pond as outlined in the Collingwood East End Drainage Study (March 2014). A 150 mm diameter sanitary service and 150 mm diameter water service will be connected to the existing infrastructure along Sandford Fleming Drive and hydro, gas and telecommunications companies all have existing services in the immediate area.

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Intern Engineer

Reviewed by: Randy Simpson, B.A.Sc., P.Eng. Senior Engineer, Group Leader

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APPENDIX A: SERVICING CALCULATIONS



		Project:	Medibudz Collingwood	Designed: AS culations	
ociates L		File No.:	118076	Designed:	AS
Orillia	Barrie		Impervious Area Calculations		
		Subject:	(Industrial Subdivision)	Checked:	RS

Site Area (Medibudz Undeveloped)	=	137,000.0 sq.m
Lot Area	=	137,000.0 sq.m
Lot Impervious Area	=	55,000.0 sq.m
Lot Pervious Area	=	82,000.0 sq.m
Directly Connected Area	=	55,000.0 sq.m
% Impervious	=	40.1%
% Directly Connected	=	40.1%
10 2 11 00 11 10 10 10 10 10 10 10 10 10 10		101170
Site Area (Medibudz Developed)	=	137,000.0 sq.m
Lot Area	=	137,000.0 sq.m
Lot Impervious Area	=	65,000.0 sq.m
Lot Pervious Area	=	72,000.0 sq.m
Directly Connected Area	=	65,000.0 sq.m
% Impervious	=	47.4%

# TOWN OF COLLINGWOOD - INDUSTRIAL PARK SWMF RETROFIT LAKE SIMCOE / SOUTH-EASTERN GEORGIAN BAY CLEAN-UP FUND INDUSTRIAL SWMF IMPROVEMENTS CALCULATIONS

#### PHOSPHORUS REMOVAL CALCULATIONS

#### SIMPLIFIED DESIGN APPROACH

Total:

#### **ESTIMATED PHOSPHORUS LOADING ESTIMATED PHOSPHORUS REMOVAL** Catchment Area (ha): 13.7 SWMF - Dry Pond SWMF - Wetland 45% Percent Impervious (%): EPA MOE Stokes Impervious Area (ha): 6.2 BMP Implemented: Dry Pond BMP Implemented: Wetland Wetland Wetland Pervious Area (ha): 7.5 Storage Volume (cu.m): 1392 Storage Volume (cu.m): 1700 1700 1700 Land Use: Industrial Treated Volume (mm): 26.8 Treated Volume (mm): 32.5 32.5 32.5 P Loading Rate (lb/acre/year): Treated Volume (inch): 1.1 Treated Volume (inch): 1.3 1.3 1.3 Impervious Area: 1.78 Performance Rating (%): 12.0% Performance Rating (%): 60.0% 70.0% 91.9% Pervious Area: 0.27 P Loading Reduction (kg/year): P Loading Reduction (kg/year): P Loading Rate (kg/ha/year): Total: 1.75 8.75 Total: 10.21 13.40 2.00 Impervious Area: Pervious Area: 0.30 Phosphorus Load (kg/year): Phosphorus Load (kg/year): Total: 12.83 Total: 5.83 4.37 1.18 Phosphorus Load (kg/year): P Reduction (kg/year): 12.30 Impervious Area: 8.46 11.65 7.00 Pervious Area: 2.28 P Loading Reduction 55% 66% 91%

Source: 1) Loading Rates - Environmental Protection Agency (April, 2012)

14.58

<sup>2)</sup> Storage Volume - Calculated from available topographical survey

<sup>3)</sup> Treated Volume - Visual OTTHYMO Hydrologic Model (CCTA, 2012)

<sup>4)</sup> Dry Pond and Wetland Performance Rating - Environmental Protection Agency (April, 2012).

# TOWN OF COLLINGWOOD - INDUSTRIAL PARK SWMF RETROFIT LAKE SIMCOE / SOUTH-EASTERN GEORGIAN BAY CLEAN-UP FUND INDUSTRIAL SWMF IMPROVEMENTS CALCULATIONS

### SEDIMENT REMOVAL CALCULATIONS

### SIMPLIFIED DESIGN APPROACH

ESTIMATED SEDIMENT LOADI	NG	ESTIMATED SEDIMENT REMO	VAL				
Catchment Area (ha):	13.7	SWMF - Dry Pond		SWMF - Wetland			
Percent Impervious (%):	45%				EPA	MOE	Stokes
Land Use:	Industrial	BMP Implemented:	Dry Pond	BMP Implemented:	Wetland	Wetland	Wetland
TSS Loading Rate (kg/ha/ye	ar):	Storage Volume (cu.m):	1392	Storage Volume (cu.m):	1700	1700	1700
Impervious Area:	770	Treated Volume (mm):	26.8	Treated Volume (mm):	32.5	32.5	32.5
		Treated Volume (inch):	1.1	Treated Volume (inch):	1.3	1.3	1.3
		Performance Rating (%):	12.0%	Performance Rating (%):	60.0%	70.0%	91.9%
TSS Loading Rate (kg/year):							
Impervious Area:	10,549	TSS Loading Reduction (ton	is/year):	TSS Loading Reduction (tons/	year):		
		Total:	1.27	Total:	6.33	7.38	9.69
Sediment Load (tons/year):							
Total:	10.55	Sediments Load (tons/year)	):	Sediment Load (tons/year):			
		Total:	9.28	Total:	4.22	3.16	0.85
				TSS Reduction (tons/year):	5.06	6.12	8.43
				TSS Loading Reduction	55%	66%	91%

Source: 1) Loading Rates - MOE SWMF Design Criteria (March 2003).

<sup>2)</sup> Storage Volume - Calculated from available topographical survey.

<sup>3)</sup> Treated Volume - Visual OTTHYMO Hydrologic Model (CCTA, 2012).

<sup>4)</sup> Dry Pond and Wetland Performance Rating - Environmental Protection Agency (April, 2012).



Project:	Medibudz	Date:	September 2018
File No.:	118076	Designed By:	AS
Subject:	Modified Rational Calculation	Checked By:	RS

### South Ditch

#### Runoff Coefficient (Municipal Standard) 0.60 2 Year 0.60 5 Year 0.60 10 Year $=C_5*1.10$ 25 Year 0.66 50 Year 0.72 $=C_5*1.20$ $=C_5*1.25$ 100 Year 0.75 Peak Rainfall Intensity MOE IDF Curve Look-Up 2 YR 5 YR 10 YR 25 YR 50 YR 100 YR **A** 21.0 27.8 32.4 38.0 42.3 46.4 B -0.699 -0.699 -0.699 -0.699 -0.699 2 Year 73.48 mm/hr $T_C = 10$ 97.27 mm/hr $T_C = 10$ 5 Year $T_C = 10$ 10 Year 113.36 mm/hr $T_C = 10$ 25 Year 132.96 mm/hr $T_C = 10$ 148.00 mm/hr 50 Year 100 Year 162.35 mm/hr $T_C = 10$ 2.250 ha Drainage Area Peak Runoff Rate - Rational Method (Q=CiA/360) $0.276 \text{ m}^3/\text{s}$ 2 Year $0.365 \text{ m}^3/\text{s}$ 5 Year $0.425 \text{ m}^3/\text{s}$ 10 Year $0.548 \text{ m}^3/\text{s}$ 25 Year $0.666 \, \text{m}^3/\text{s}$ 50 Year 0.761 m<sup>3</sup>/s 100 Year

### **North Ditch**

Runoff Coefficient			1unicipa	al Standa	rd)		
2 Year	0.63						
5 Year	0.63						
10 Year	0.63						
25 Year	0.69	=(	C <sub>5</sub> *1.10	)			
50 Year	0.76	=(	C <sub>5</sub> *1.20	)			
100 Year	0.79	=(	C <sub>5</sub> *1.25	j			
Peak Rain	fall Intensity		MOI	E IDF Cur	ve Look-	Up	
	2 YR 5	YR 1	0 YR	25 YR	50 YR	100	YR
Α	21.0 2	7.8	32.4	38.0	42.3	46	.4
В	-0.699 -0	.699 -	0.699	-0.699	-0.699	-0.6	99
2 Year	71	3.48 m	m/hr		Tc	_	10
5 Year		7.27 m			Tc		10
10 Year	11	3.36 m	m/hr		Tc		10
25 Year		2.96 m				=	
50 Year	14	8.00 m	m/hr			=	
100 Year	16	2.35 m	m/hr		T <sub>C</sub>		10
	•	0.700					
<u>Drainage</u> <i>I</i>	<u>Area</u>	0.780	) ha				
Peak Run	off Rate - Ra	ntional M	<u>ethod</u>		(Q=CiA/	360)	
2 Year	0.100	m³/s					
5 Year	0.133						
10 Year	0.155						
25 Year	0.200	2					
50 Year	0.242						

### **Manning's Equations**

$$Q = \frac{1}{n} \cdot A \cdot R^{2/3} \cdot S^{1/2}$$

Cross-Section A-A		Cross-Section D-D	
Channel		Channel	
Manning's n	0.04	Manning's n	0.04
Slope	0.01 m/m	Slope	0.01 m/m
Bottom Width	0.00 m	Bottom Width	2.00 m
Side Slopes	3.00 :1	Side Slopes	3.00 :1
Depth	0.49 m	Depth	0.87 m
Slope Width	1.47	Slope Width	2.61
Area	$0.72 \text{ m}^2$	Area	4.01 m <sup>2</sup>
Perimeter	3.10 m	Perimeter	7.50 m
Hydraulic Radius	0.23 m	Hydraulic Radius	0.53 m
Flow	<b>0.81</b> m <sup>3</sup> /s	Flow	<b>6.60</b> m <sup>3</sup> /s
Cross-Section B-B		Cross-Section F-F	
Channel		Channel	
Manning's n	0.04	Manning's n	0.04
Slope	0.01 m/m	Slope	0.01 m/m
Bottom Width	0.00 m	Bottom Width	0.00 m
Side Slopes	3.00:1	Side Slopes	5.00:1
Depth	0.83 m	Depth	0.50 m
Slope Width	2.49	Slope Width	2.50
Area	2.07 m <sup>2</sup>	Area	1.25 m <sup>2</sup>
Perimeter	5.25 m	Perimeter	5.10 m
Hydraulic Radius	0.39 m	Hydraulic Radius	0.25 m
Flow	<b>2.78</b> m <sup>3</sup> /s	Flow	<b>1.22</b> m <sup>3</sup> /s
Cross-Section C-C		Cross-Section G-G	
Channel		Channel	
Manning's n	0.04	Manning's n	0.04
Slope	0.01 m/m	Slope	0.01 m/m
Bottom Width	0.00 m	Bottom Width	0.00 m
Side Slopes	6.00:1	Side Slopes	10.00 :1
Depth	0.50 m	Depth	0.40 m
Slope Width	3.00	Slope Width	4.00
Area	1.50 m <sup>2</sup>	Area	1.60 m <sup>2</sup>
Perimeter	6.08 m	Perimeter	8.04 m
Hydraulic Radius	0.25 m	Hydraulic Radius	0.20 m
Flow	<b>1.47</b> m <sup>3</sup> /s	Flow	<b>1.56</b> m <sup>3</sup> /s

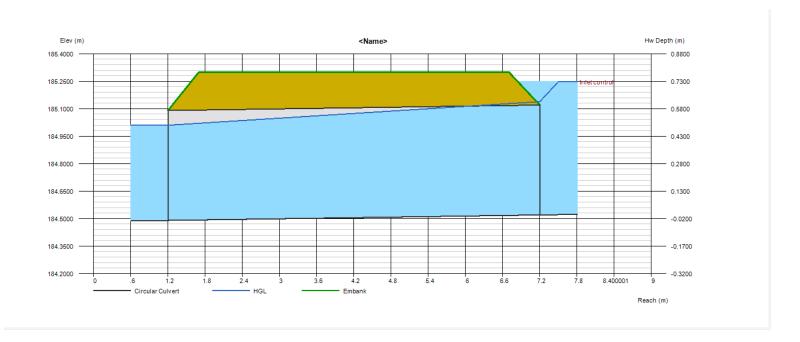
# **Culvert Report**

Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

Friday, Sep 28 2018

### **Circular Culvert**

Invert Elev Dn (m)	= 184.4900	Calculations	
Pipe Length (m)	= 6.0000	Qmin (cms)	= 0.0000
Slope (%)	= 0.4998	Qmax (cms)	= 2.0000
Invert Elev Up (m)	= 184.5200	Tailwater Elev (m)	= (dc+D)/2
Rise (mm)	= 600.0		
Shape	= Circular	Highlighted	
Span (mm)	= 600.0	Qtotal (cms)	= 0.4500
No. Barrels	= 1	Qpipe (cms)	= 0.4500
n-Value	= 0.024	Qovertop (cms)	= 0.0000
Culvert Type	<ul> <li>Circular Corrugate Metal Pipe</li> </ul>	Veloc Dn (m/s)	= 1.7294
Culvert Entrance	= Headwall	Veloc Up (m/s)	= 1.5915
Coeff. K,M,c,Y,k	= 0.0078, 2, 0.0379, 0.69, 0.5	HGL Dn (m)	= 185.0097
		HGL Up (m)	= 185.1384
Embankment		Hw Elev (m)	= 185.2475
Top Elevation (m)	= 185.3000	Hw/D (m)	= 1.2125
Top Width (m)	= 5.0000	Flow Regime	= Inlet Control
Crest Width (m)	= 5.0000		



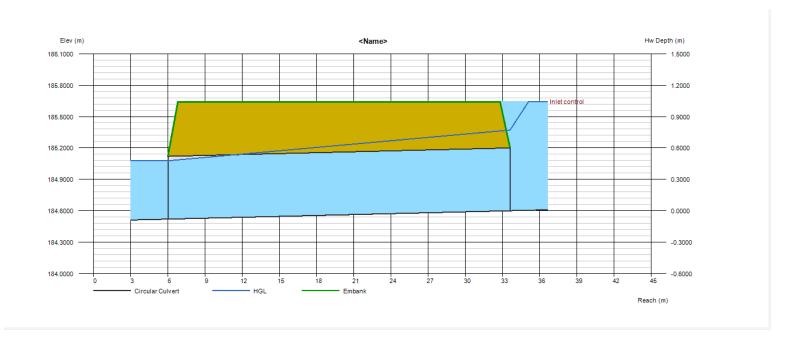
# **Culvert Report**

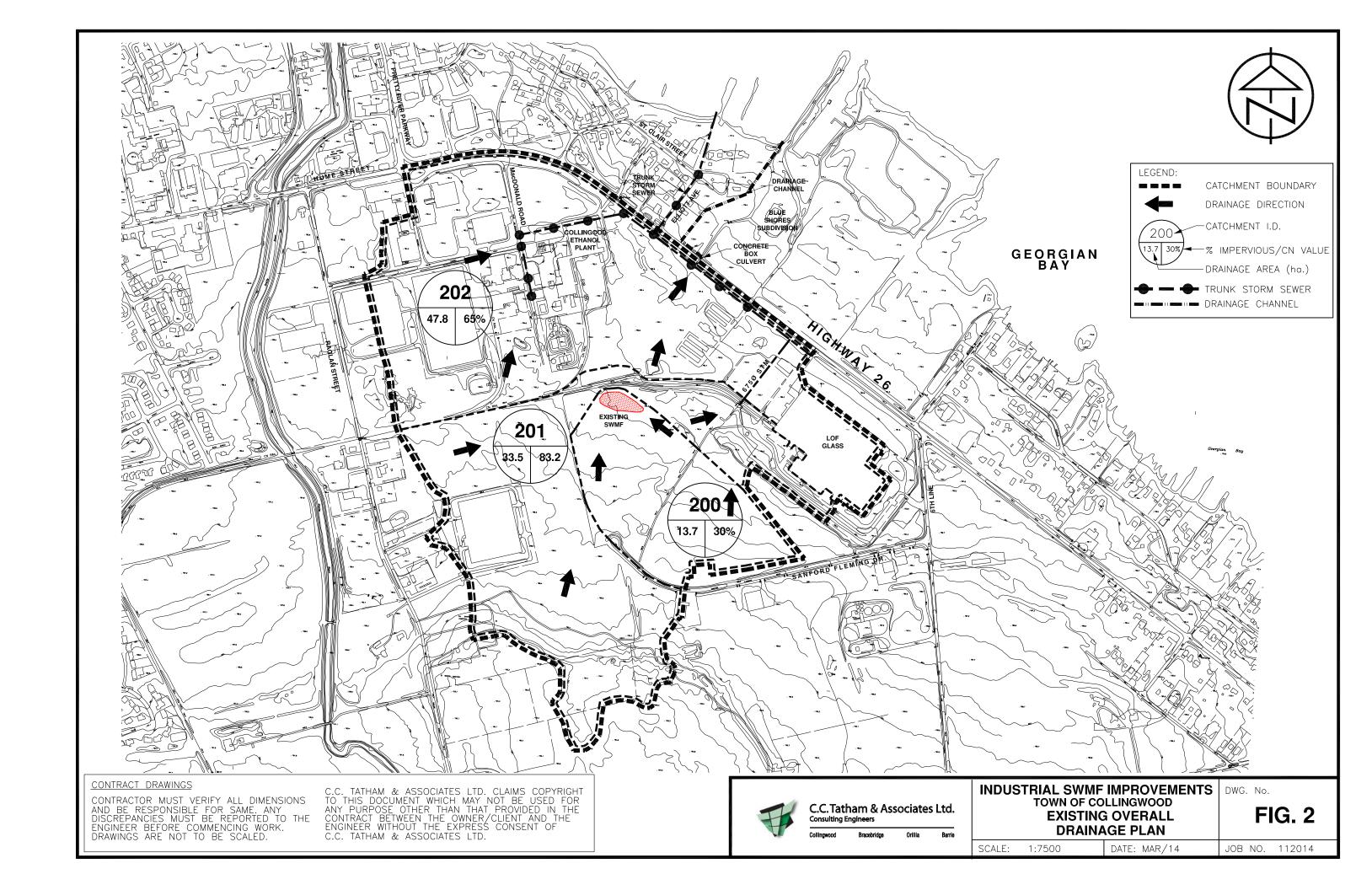
Hydraflow Express Extension for Autodesk® AutoCAD® Civil 3D® by Autodesk, Inc.

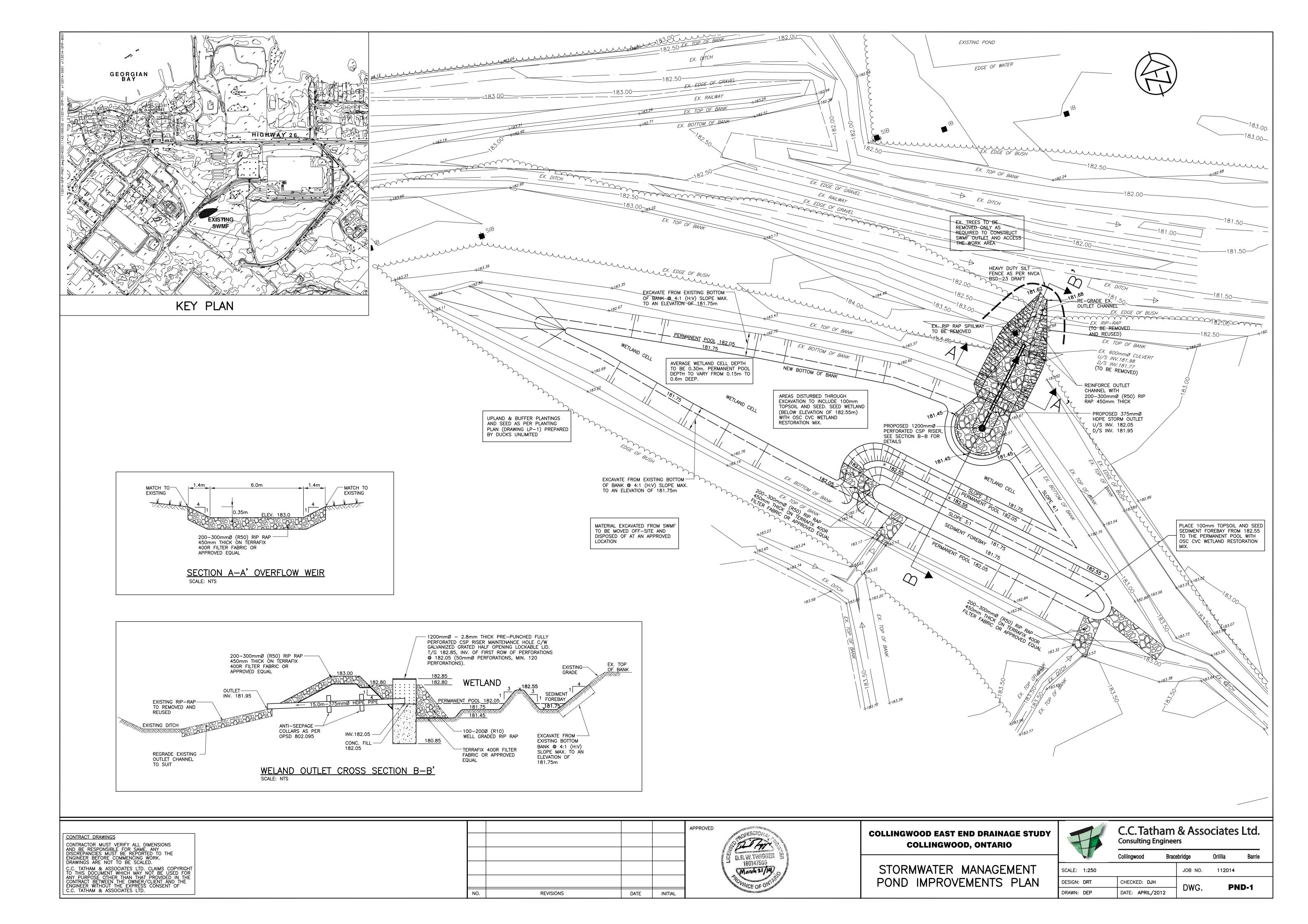
Monday, Oct 1 2018

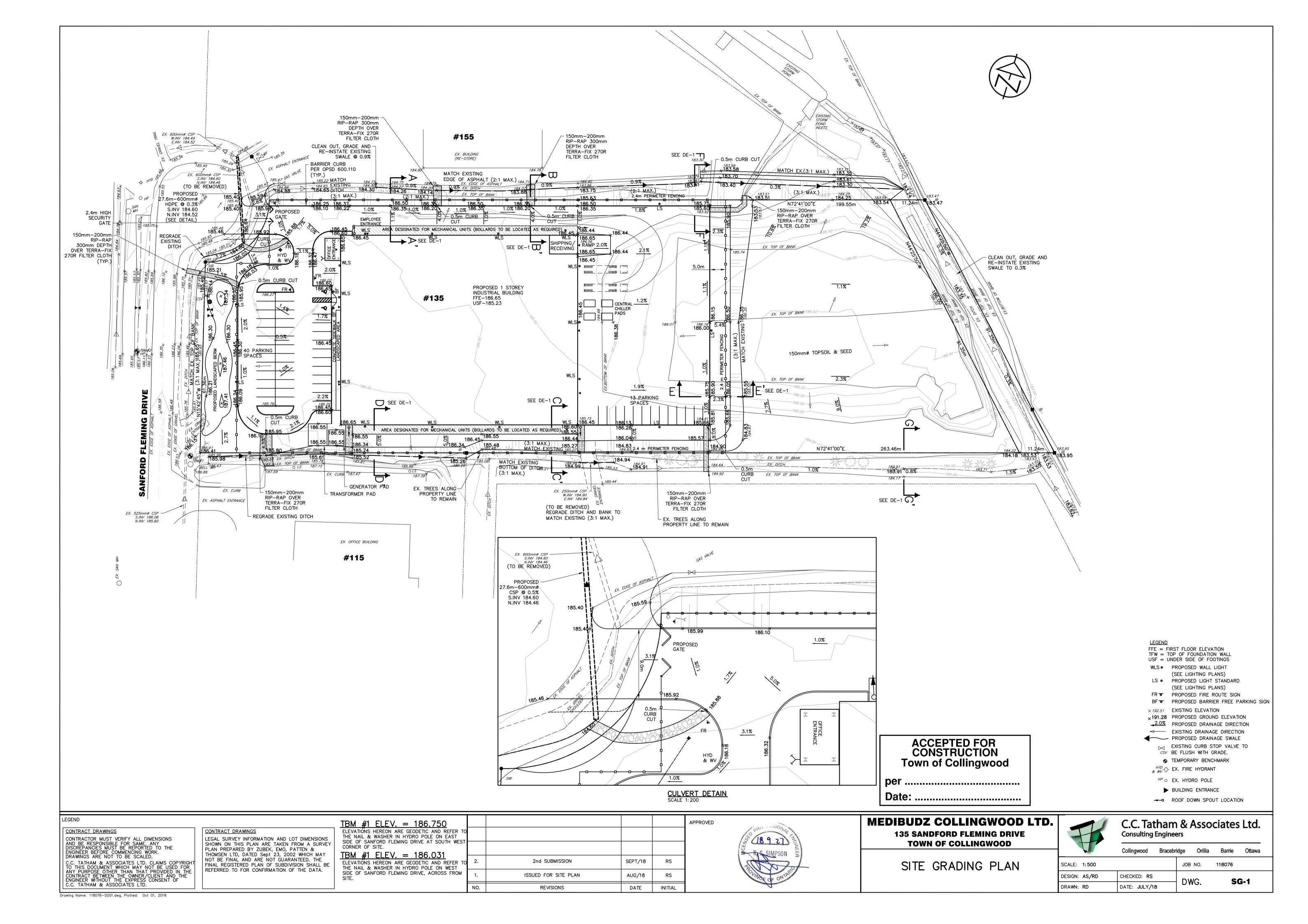
### **Circular Culvert**

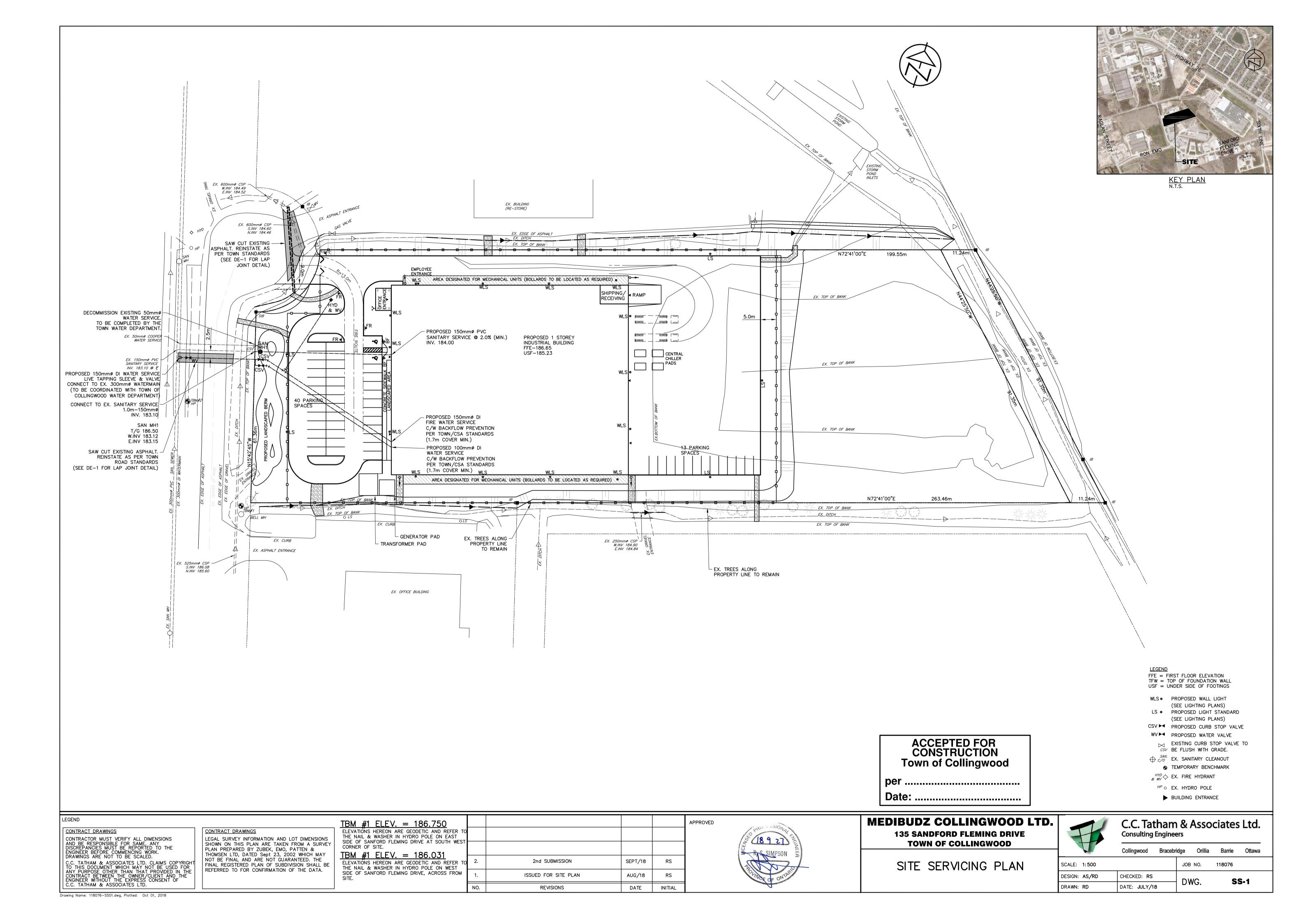
Invert Elev Dn (m)	= 184.5200	Calculations	
Pipe Length (m)	= 27.6000	Qmin (cms)	= 0.0000
Slope (%)	= 0.2899	Qmax (cms)	= 2.0000
Invert Elev Up (m)	= 184.6000	Tailwater Elev (m)	= (dc+D)/2
Rise (mm)	= 600.0		
Shape	= Circular	Highlighted	
Span (mm)	= 600.0	Qtotal (cms)	= 0.6500
No. Barrels	= 1	Qpipe (cms)	= 0.6365
n-Value	= 0.013	Qovertop (cms)	= 0.0135
Culvert Type	<ul> <li>Circular Corrugate Metal Pipe</li> </ul>	Veloc Dn (m/s)	= 2.3241
Culvert Entrance	= Headwall	Veloc Up (m/s)	= 2.2512
Coeff. K,M,c,Y,k	= 0.0078, 2, 0.0379, 0.69, 0.5	HGL Dn (m)	= 185.0775
		HGL Up (m)	= 185.3712
Embankment		Hw Elev (m)	= 185.6433
Top Elevation (m)	= 185.6400	Hw/D (m)	= 1.7388
Top Width (m)	= 26.0000	Flow Regime	= Inlet Control
Crest Width (m)	= 26.0000		

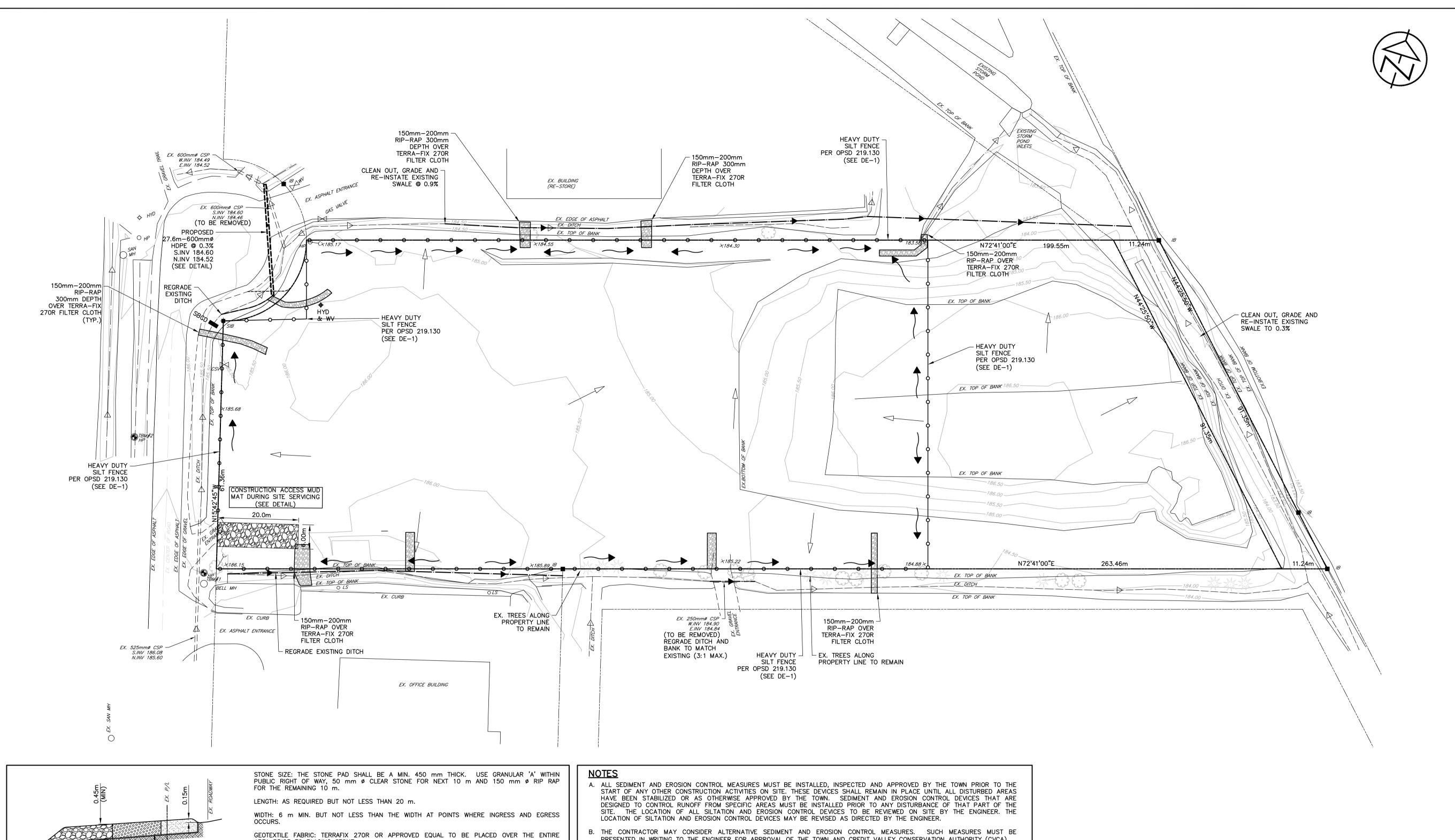


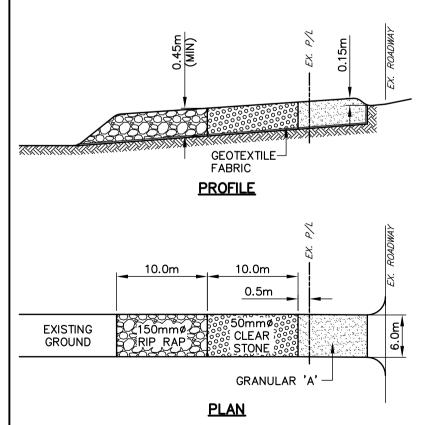












AREA PRIOR TO PLACING STONE.

SURFACE WATER: ALL SURFACE WATER FLOWING OR DIRECTED TOWARD CONSTRUCTION ENTRANCES SHALL BE DIRECTED ACROSS THE ENTRANCE THROUGH A TEMPORARY CULVERT,

MAINTENANCE: THE CONTRACTOR SHALL MAINTAIN THE ENTRANCE IN A CONDITION WHICH WILL PREVENT TRACKING OR FLOWING OF SEDIMENT ONTO THE PUBLIC RIGHT-OF-WAY. THIS MAY REQUIRE PERIODIC DRESSING WITH ADDITIONAL STONE AS CONDITIONS DEMAND AND REPAIR AND/OR CLEANOUT OF ANY MEASURES USED TO TRAP SEDIMENT. ALL SEDIMENT SPILLED, DROPPED, WASHED OR TRACKED ONTO THE PUBLIC RIGHT-OF-WAY MUST BE REMOVED IMMEDIATELY BY THE CONTRACTOR. UPON OBSERVATION OF CONTINUOUS MUD TRACKING ONTO ADJACENT STREETS, THE STONE MAT IS TO BE FULLY REPLACED.

WASHING: WHEELS SHALL BE CLEANED TO REMOVE SEDIMENT PRIOR TO ENTRANCE ONTO THE PUBLIC RIGHT-OF-WAY. WHEN WASHING IS REQUIRED, IT SHALL BE DONE ON AN AREA STABILIZED WITH STONE AND WHICH DRAINS INTO AN APPROVED SEDIMENT TRAPPING DEVICE. INSPECTION & MAINTENANCE: REQUIRED MAINTENANCE AFTER EACH RAIN EVENT SHALL BE PROVIDED BY THE CONTRACTOR.

CONSTRUCTION ACCESS MUD MAT TO BE REMOVED UPON COMPLETION OF SITE SERVICING AND

CONSTRUCTION ACCESS MUD MAT DETAIL

- PRESENTED IN WRITING TO THE ENGINEER FOR APPROVAL OF THE TOWN AND CREDIT VALLEY CONSERVATION AUTHORITY (CVCA).
- THE CONTRACTOR SHALL HAVE MATERIALS AVAILABLE ON-SITE TO REPAIR SEDIMENT AND EROSION CONTROL DEVICES IN THE EVENT OF UNFORESEEN CONDITIONS: HIGH WATER, EXTREME RAINFALL EVENTS, ETC.
- D. ALL EROSION AND SEDIMENT CONTROL DEVICES MUST BE INSPECTED, CLEANED AND MAINTAINED BY THE CONTRACTOR AFTER EACH STORM EVENT. ALL WORKS WILL BE INSPECTED BY THE ENGINEER BI-WEEKLY AND AFTER EACH MAJOR STORM EVENT.
- . CONSTRUCTION OF ALL SILTATION AND EROSION CONTROL WORKS ARE TO BE IN ACCORDANCE WITH THE FOLLOWING STEPS: INSTALL STONE MUD MAT AS PER DETAIL.
- 2. INSTALL SILT FENCE AS PER OPSD 219.130. 3. INSTALL STRAW BALE FLOW CHECKS AS PER OPSD 219.180.
- ALL CONSTRUCTION VEHICLES TO ACCESS SITE USING THE DESIGNATED CONSTRUCTION ENTRANCES.
- G. EROSION AND SEDIMENT CONTROL DEVICES TO BE REMOVED BY THE CONTRACTOR ONCE GROUND COVER IS ESTABLISHED AND LANDSCAPING IS COMPLETE AND APPROVED BY THE ENGINEER.

APPROVED

- H. STOCKPILE LOCATIONS ARE TO BE APPROVED BY THE ENGINEER.
- PROVIDE SNOW FENCE OR APPROVED EQUAL ACROSS ALL CONSTRUCTION ENTRANCES DURING PERIODS OF INACTIVITY.
- J. CONSTRUCTION AREAS THAT EXCEED 30 DAYS OF INACTIVITY SHALL BE STABILIZED BY SEEDING.

# **ACCEPTED FOR** CONSTRUCTION **Town of Collingwood**

per ..... Date: .....

# <u>LEGEND</u>

× 192.51 EXISTING ELEVATION → EXISTING DRAINAGE DIRECTION

SBCD PROPOSED STRAW BALE CHECK DAM 

\* WV - EX. FIRE HYDRANT <sup>HP</sup> ○ EX. HYDRO POLE TEMPORARY SWALE

LEGEND CONTRACT DRAWINGS CONTRACTOR MUST VERIFY ALL DIMENSIONS AND BE RESPONSIBLE FOR SAME. ANY DISCREPANCIES MUST BE REPORTED TO THE ENGINEER BEFORE COMMENCING WORK. DRAWINGS ARE NOT TO BE SCALED. C.C. TATHAM & ASSOCIATES LTD. CLAIMS COPYRIGHT TO THIS DOCUMENT WHICH MAY NOT BE USED FOR ANY PURPOSE OTHER THAN THAT PROVIDED IN THE CONTRACT BETWEEN THE OWNER/CLIENT AND THE ENGINEER WITHOUT THE EXPRESS CONSENT OF C.C. TATHAM & ASSOCIATES LTD.

CONTRACT DRAWINGS LEGAL SURVEY INFORMATION AND LOT DIMENSIONS SHOWN ON THIS PLAN ARE TAKEN FROM A SURVEY PLAN PREPARED BY ZUBEK, EMO, PATTEN & THOMSEN LTD, DATED Sept 23, 2002 WHICH MAY NOT BE FINAL AND ARE NOT GUARANTEED. THE FINAL REGISTERED PLAN OF SUBDIVISION SHALL BE REFERRED TO FOR CONFIRMATION OF THE DATA.

TBM #1 ELEV. = 186.750 ELEVATIONS HEREON ARE GEODETIC AND REFER THE NAIL & WASHER IN HYDRO POLE ON EAST SIDE OF SANFORD FLEMING DRIVE AT SOUTH WEST CORNER OF SITE. TBM #1 ELEV. = 186.031 2nd SUBMISSION SEPT/18 RS ELEVATIONS HEREON ARE GEODETIC AND REFER TO THE NAIL & WASHER IN HYDRO POLE ON WEST SIDE OF SANFORD FLEMING DRIVE, ACROSS FROM ISSUED FOR SITE PLAN AUG/18 RS REVISIONS DATE INITIAL



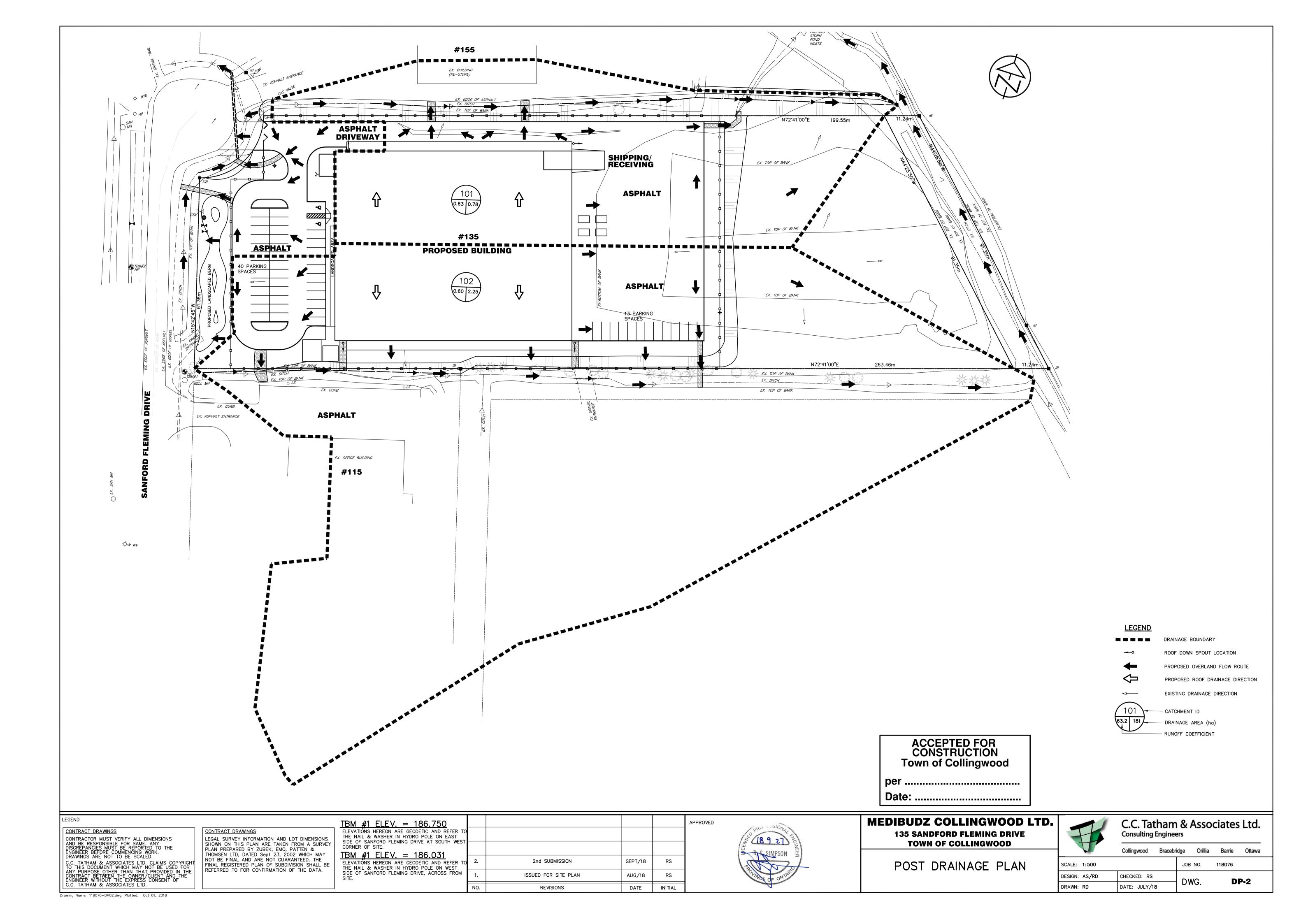
# MEDIBUDZ COLLINGWOOD LTD. 135 SANDFORD FLEMING DRIVE TOWN OF COLLINGWOOD

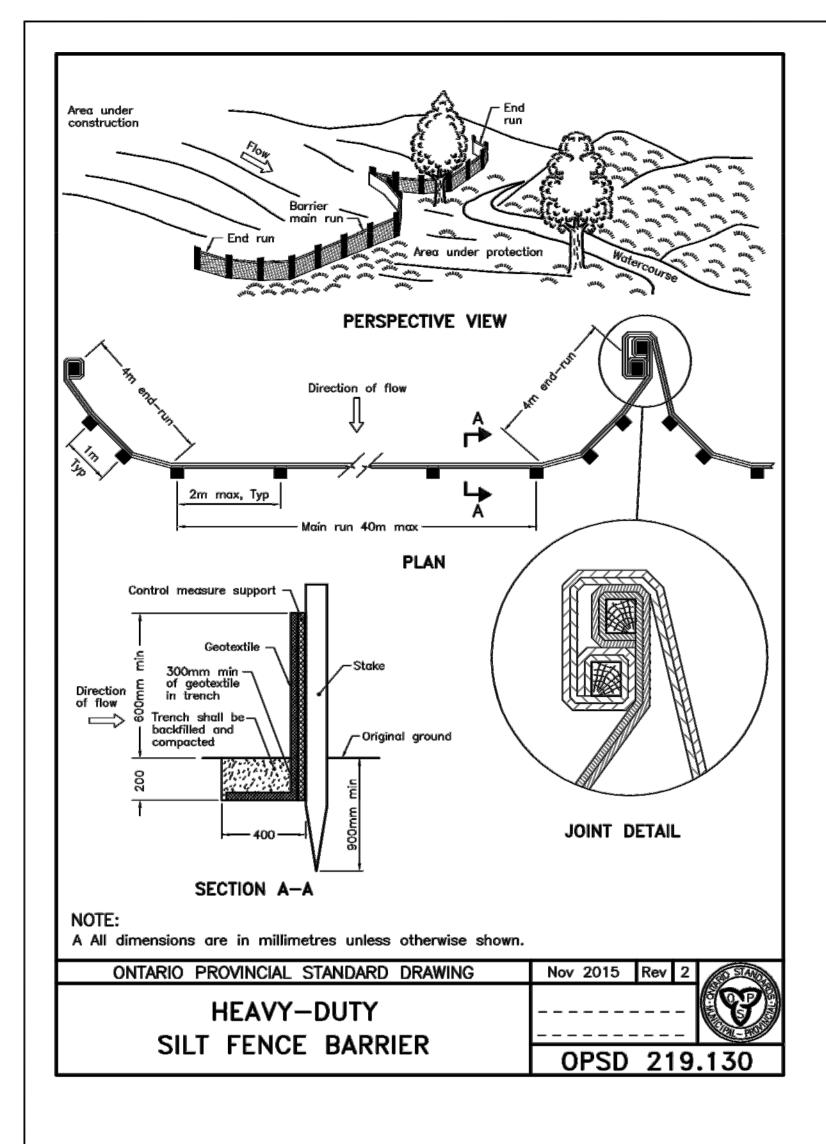
SITATION & EROSION CONTROL PLAN

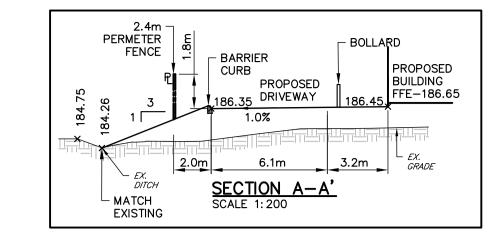


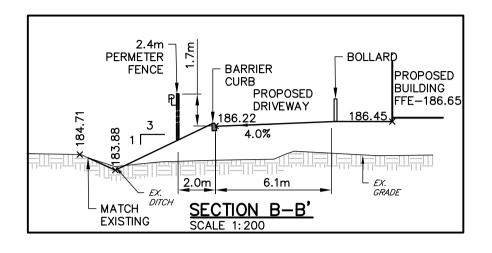
# C.C. Tatham & Associates Ltd. **Consulting Engineers**

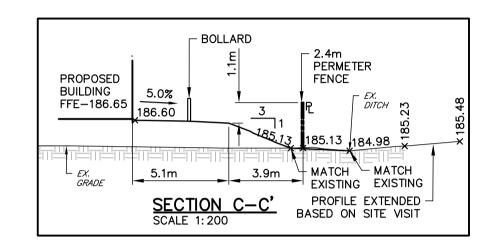
	Collingwood	Bracebr	idge	Orillia	Barrie	Ottawa
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DESIGN: AS/RD	CHECKED: RS		DV	IC	84	C-1
DRAWN: RD	DATE: JULY/18	3	DWG.			<b>G-1</b>

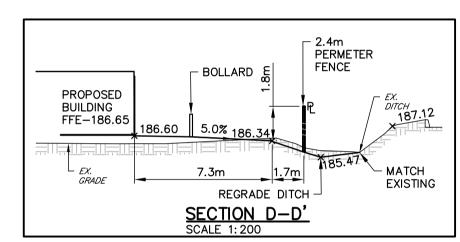


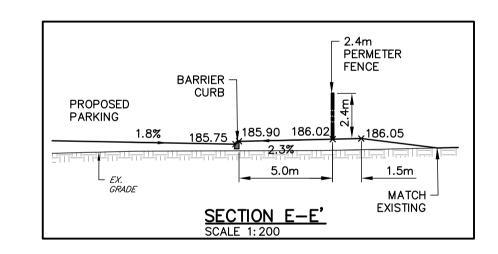


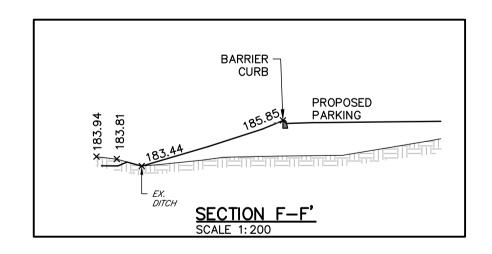


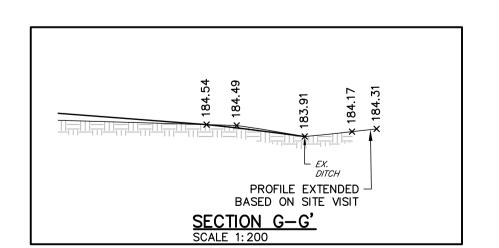












### <u>GENERAL</u>

- A. ALL WORK TO BE CARRIED OUT IN ACCORDANCE WITH TOWN OF COLLINGWOOD STANDARDS AND OPS STANDARDS. WHERE CONFLICT OCCURS, TOWN STANDARDS TO GOVERN.
- B. THE ENGINEER SHALL PROVIDE BENCHMARK ELEVATIONS. THE CONTRACTOR SHALL BE RESPONSIBLE FOR THE DETAILED LAYOUT OF THE WORK.
- C. LEGAL SURVEY BOUNDARIES SHOWN ON DRAWING ARE APPROXIMATE, CONTRACTOR SHALL CONFIRM ALL BOUNDARIES AS REQUIRED TO COMPLETE THE WORK.
- D. ALL PROPERTY BARS TO BE PRESERVED AND REPLACED BY OLS AT CONTRACTORS
- EXPENSE IF DISTURBED DURING CONSTRUCTION. E. THE CONTRACTOR SHALL MAKE ARRANGEMENTS FOR THE SUPPLY OF TEMPORARY WATER
- F. DEWATERING TO BE CARRIED OUT IN ACCORDANCE WITH OPSS 517 AND OPSS 518. MAINTAIN ALL TRENCHES IN A DRY CONDITION. A MOECC PERMIT TO TAKE WATER (PTTW) HAS NOT BEEN OBTAINED FOR THIS PROJECT. IF THE CONTRACTOR CANNOT MAINTAIN

DRY TRENCH CONDITIONS WITH CONVENTIONAL PUMP TECHNIQUES WHILE TAKING LESS

THAN 50,000 L/DAY, THEN A PTTW MUST BE OBTAINED FROM THE MINISTRY OF

- ENVIRONMENT AND CLIMATE CHANGE. G. ALL ENGINE DRIVEN PUMPS TO BE ADEQUATELY SILENCED, SUITABLE FOR OPERATION IN A RESIDENTIAL DISTRICT.
- H. GENERAL INSTALLATION AND TESTING OF SEWERS, WATERMAIN AND APPURTENANCES TO BE IN ACCORDANCE WITH OPSS.MUNI 407, 408, 409 (CCTV), OPSS.MUNI 410, OPSS.MUNI
- 421, AND 441 AND ALL SPECIFICATIONS REFERENCED WITHIN THESE SECTIONS. I. EXCAVATION AND GRADING TO BE IN ACCORDANCE WITH OPSS.MUNI 206 AND OPSS.MUNI
- J. TRENCH BACKFILL TO BE SELECT NATIVE MATERIAL OR IMPORTED SELECT SUBGRADE MATERIAL IN ACCORDANCE WITH OPSS.MUNI 1010. BACKFILL TO BE PLACED IN MAXIMUM 200 mm THICK LIFTS (OR AS OTHERWISE DIRECTED BY THE GEOTECHNICAL ENGINEER) AND COMPACTED TO A DRY DENSITY OF AT LEAST 95% OF THE MATERIAL'S STANDARD PROCTOR MAXIMUM DRY DENSITY (SPMDD).
- K. PIPE EMBEDMENT TO BE COMPACTED TO A DRY DENSITY OF AT LEAST 95% OF THE MATERIAL'S SPMDD. BACKFILL AND EMBEDMENT IN ACCORDANCE WITH OPSD 802.010 (FLEXIBLE PIPE), GRANULAR 'A' EMBEDMENT OR OPSD 802.031 (RIGID PIPE) CLASS "B", GRANULAR 'A' BEDDING, GRANULAR 'B' COVER (MAX. AGGREGATE SIZE 25 mm). MINIMUM BEDDING DEPTH 150 mm, MINIMUM COVER DEPTH 300 mm ON ALL PIPES. WHERE EXCESSIVELY WET OR POOR SUBGRADE IS ENCOUNTERED AT THE INVERT LEVEL, IT MAY BE NECESSARY TO INCREASE THE BEDDING THICKNESS.
- L. CLEAR STONE COMPLETELY WRAPPED IN FILTER FABRIC CAN BE SUBSTITUTED FOR EMBEDMENT MATERIAL IF APPROVED BY THE ENGINEER.
- M. DISTURBED AREAS TO BE REINSTATED TO PREVIOUS CONDITION OR BETTER.
- N. REINSTATEMENT OF ALL DISTURBED AREAS TO INCLUDE REGRADING, PLACEMENT OF MIN. 150 mm TOPSOIL, SEED AND MULCH IN ACCORDANCE WITH OPSS 802 AND OPSS.MUNI
- O. LOCATION OF EXISTING INFRASTRUCTURE BASED ON A TOPOGRAPHICAL SURVEY COMPLETED BY C.C. TATHAM & ASSOCIATES LTD., AS-BUILT DRAWINGS AND/OR GIS INFORMATION PROVIDED BY THE TOWN.
- P. LOCATIONS OF EXISTING UTILITIES ARE NOT GUARANTEED. THE CONTRACTOR SHALL OBTAIN LOCATES FROM ALL RELEVANT UTILITY COMPANIES, 48 HOURS PRIOR TO THE
- COMMENCEMENT OF ANY WORK AND IF NECESSARY LOCATE UTILITIES BY HAND DIGGING. Q. THE CONTRACTOR IS RESPONSIBLE FOR THE PRESERVATION OF ALL EXISTING INFRASTRUCTURE/FACILITIES AS WELL AS NOTIFYING ALL UTILITY COMPANIES PRIOR TO
- COMMENCING WORK AND CO-ORDINATE CONSTRUCTION ACCORDINGLY. R. ALL ON-SITE MATERIAL SHALL BE PROPERLY STORED, SECURED, MONITORED AND COVERED
- AS REQUIRED. SPECIFICALLY, ALL PVC PIPE SHALL BE COVERED WHILE STORED ON-SITE. S. ALL SILTATION & EROSION CONTROL PROTECTION DEVICES ARE TO BE INSTALLED PRIOR TO COMMENCEMENT OF CONSTRUCTION. CONTRACTOR SHALL MAINTAIN CONTROL DEVICES THROUGHOUT CONSTRUCTION AND REMOVE THE CONTROL DEVICES ONCE GROUND COVER IS
- T. ALL CONSTRUCTION MATERIALS SHALL BE REMOVED FROM THE SITE PRIOR TO RESTORATION OF DISTURBED AREAS.
- U. ALL SIGNAGE TO BE LAWFULLY ERECTED AND MAINTAINED IN ACCORDANCE TO THE TOWN
- V. ALL FENCING TO BE LAWFULLY ERECTED AND MAINTAINED IN ACCORDANCE TO THE TOWN FENCE BYLAW.
- W. CLEARING, GRUBBING AND REMOVAL OF SURFACE BOULDERS TO OPSS 201.
- X. GRADING TO OPSS.MUNI 206. Y. COMPACTING TO OPSS.MUNI 501.

ESTABLISHED IN ALL DISTURBED AREAS.

# ROADS/PARKING AREAS

- A. SUBGRADE AND BOULEVARD MATERIAL TO BE COMPACTED TO A DRY DENSITY OF AT LEAST 95% OF THE MATERIAL'S SPMDD. SUBGRADE TO BE PROOF ROLLED AND CERTIFIED PRIOR TO PLACING GRANULAR 'B'. FILL PLACED WITHIN 3.0 m OF AND WITHIN THE BUILDING ENVELOPE TO BE COMPACTED TO A DRY DENSITY OF AT LEAST 98% OF THE MATERIAL'S SPMDD, UNDER FULL TIME SUPERVISION OF THE GEOTECHNICAL CONSULTANT.
- B. GRANULAR 'A' AND 'B' TO BE COMPACTED TO A DRY DENSITY OF AT LEAST 100% OF THE MATERIAL'S RESPECTIVE SPMDD.
- C. ALL GRANULARS AND ASPHALT MATERIAL TO BE PLACED IN ACCORDANCE WITH OPSS 310 AND OPSS.MUNI 314.
- D. ASPHALT TO BE COMPACTED TO A MINIMUM OF 92% OF THE MATERIAL'S MAXIMUM RELATIVE
- E. FRONT PARKING AREA TO BE CONSTRUCTED WITH MIN. 300 mm GRANULAR 'B'. 150 mm
- GRANULAR 'A', 50mm HL8 AND 40mm HL3.
- F. ENTRANCE THROUGH TO REAR PARKING AREA TO BE CONSTRUCTED WITH MIN. 400mm GRANULAR 'B', 200mm GRANULAR 'A', 90mm HL8 AND 40mm HL13.
- G. JOINTS WITH EXISTING ASPHALT TO BE SAW CUT STRAIGHT PRIOR TO PLACING NEW ASPHALT AND TACK COAT SHALL BE APPLIED TO EXISTING ASPHALT. WHERE EXISTING ASPHALT IS GREATER THAN 75 mm DEPTH, A 300 mm WIDE BY 40 mm DEEP LAP JOINT SHALL BE GROUND INTO EXISTING ASPHALT, OTHERWISE A BUTT JOINT SHALL BE USED.
- H. SELECT SUBGRADE MATERIAL, OR IMPORTED GRANULAR MATERIAL APPROVED BY THE ENGINEER, COMPACTED TO 98% S.P.M.D.D. TO BE USED AS FILL IN ALL AREAS WHERE PROPOSED PIPE INVERTS ARE HIGHER THAN EXISTING GRADE OR AS INSTRUCTED BY THE ENGINEER.
- I. TACK COAT TO BE APPLIED AT THE DIRECTION OF THE ENGINEER.
- J. CONCRETE BARRIER CURB IN ACCORDANCE WITH OPSD 600.110 AND OPSS 353. CONCRETE SIDEWALK IN ACCORDANCE WITH OPSD 310.020 AND OPSS 351. SUBBASE TO CONSIST OF 150 mm DEPTH GRANULAR 'A'.
- K. ALL FIRE ROUTE SIGNAGE TO BE AS PER TOWN OF COLLINGWOOD BY-LAW 96-37.
- L. BOLLARDS TO BE 100 mm DIA. SCH 40 (RAW PIPE) AND FILLED WITH CONCRETE. BASE TO BE SET AT A MINIMUM OF 1.22 m BELOW GRADE. TOP TO BE SET MIN. 1.2 m ABOVE GRADE. PLASTIC BOLLARD COVER TO BE PROVIDED, YELLOW IN COLOUR.
- M. RIP-RAP AT CURB CUTS IN ACCORDANCE WITH OPSD 810.010

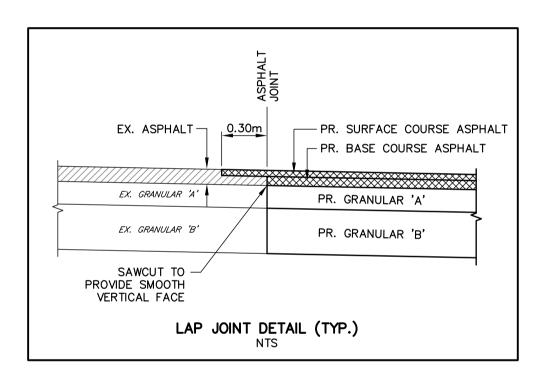
### SANITARY SERVICE

A. SERVICE CONNECTION IN ACCORDANCE WITH OPSD 1006.020, 150 mm DIAMETER, TERMINATED WHERE SPECIFIED ON THE DRAWING COMPLETE WITH PLUG AND MARKED WITH A 38mm X 89mm POST PAINTED GREEN FROM THE INVERT OF THE SERVICE TO 600 mm ABOVE GRADE. , GRANULAR 'A' EMBEDMENT (MIN. 150 mm BEDDING AND 300 mm

### <u>WATERMAIN</u>

- A. ALL WORK ON TOWN PROPERTY AND ON TOWN OF COLLINGWOOD WATER DEPARTMENT WATER MAINS MUST BE UNDERTAKEN BY THE TOWNS WATER DEPARTMENT OR BY AN APPROVED CONTRACTOR WITH THE TOWNS WATER DEPARTMENT APPROVAL, ALL AT THE DEVELOPER'S COST.
- B. ALL SERVICES ARE TO BE CONSTRUCTED IN ACCORDANCE WITH THE TOWN OF COLLINGWOOD WATER DEPARTMENT STANDARDS.
- C. SERVICE CONNECTIONS TO OPSD 1104.010 LIVE TAP, GRANULAR 'A' EMBEDMENT (200 mm BEDDING AND 300 mm COVER).
- D. MINIMUM COVER ON WATER SERVICE TO BE 1.7 m.
- E. BACKFLOW PREVENTION DEVICES AS PER CSA B64.10-11/B64.10.1-11, OBC AND TOWN WATER BY-LAW TO BE INSTALLED INTERNAL TO THE BUILDING AND CERTIFIED BY THE CONTRACTOR AND A COPY OF THE CERTIFICATE OF PASSING PROVIDED TO THE TOWN.
- TESTING OF THE BACKFLOW PREVENTION DEVICES IS AN ANNUAL REQUIREMENT. F. NO WATER VALVES SHALL BE OPERATED WITHOUT THE APPROVAL OF THE TOWN OF COLLINGWOOD WATER DEPARTMENT.
- G. THE MUNICIPALITY WILL HAVE ONE METER, CONNECTED TO ONE WATER BILL

- A. ALL MATERIAL TO COMPLY WITH CSA, OPSS AND TOWN STANDARDS.
- B. SANITARY SERVICE CONNECTIONS PVC SDR 28 (GREEN).
- C. AGGREGATES IN ACCORDANCE WITH OPSS.MUNI 1010.
- D. FILTER FABRIC TERRAFIX 270R OR APPROVED EQUAL. E. WATER SERVICES TO BE DUCTILE IRON.
- F. MAIN STOPS CAMBRIDGE BRASS 201-A3H3 (AWWA THREAD BY COMPRESSION)
- G. CURB STOPS CAMBRIDGE BRASS 203-H3H3 (AWWA THREAD BY COMPRESSION). H. SERVICE BOXES - CLOW OR MUELLER #7 OR #8 D-I WITH 24" STAINLESS STEEL ROD,
- I. LIVE TAP SADDLES EPOXY COATED C/W STAINLESS STEEL BOLTS. J. LIVE TAP VALVE - RESILIENT SEATED RSGV, LIVE TAP VALVE, OPEN LEFT CLOW OR
- K. CULVERTS SMOOTH WALL HDPE (MIN. PIPE STIFFNESS = 320 kPa) OR CORRUGATED
  - METAL PIPE (MIN. THICKNESS = 2.0 mm)
- L. RIP RAP TO OPSD 1004.05.06



**ACCEPTED FOR** CONSTRUCTION **Town of Collingwood** 

per ..... Date: .....

MEDIBUDZ COLLINGWOOD LTD. 135 SANDFORD FLEMING DRIVE **TOWN OF COLLINGWOOD** 

DETAILS & NOTES



DRAWN: RD

C.C. Tatham & Associates Ltd. **Consulting Engineers** 

DWG.

DE-1

Orillia Bracebridge Barrie Collingwood SCALE: AS SHOWN JOB NO. 118076 DESIGN: AS/RD CHECKED: RS

DATE: JULY/18

LEGEND CONTRACT DRAWINGS CONTRACTOR MUST VERIFY ALL DIMENSIONS AND BE RESPONSIBLE FOR SAME. ANY DISCREPANCIES MUST BE REPORTED TO THE ENGINEER BEFORE COMMENCING WORK. DRAWINGS ARE NOT TO BE SCALED. C.C. TATHAM & ASSOCIATES LTD. CLAIMS COPYRIG TO THIS DOCUMENT WHICH MAY NOT BE USED FOR ANY PURPOSE OTHER THAN THAT PROVIDED IN THE CONTRACT BETWEEN THE OWNER/CLIENT AND THE ENGINEER WITHOUT THE EXPRESS CONSENT OF C.C. TATHAM & ASSOCIATES LTD.

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CORNER OF SITE. TBM #1 ELEV. = 186.031 ELEVATIONS HEREON ARE GEODETIC AND REFER THE NAIL & WASHER IN HYDRO POLE ON WEST SIDE OF SANFORD FLEMING DRIVE, ACROSS FROM

TBM #1 ELEV. = 186.750ELEVATIONS HEREON ARE GEODETIC AND REFER THE NAIL & WASHER IN HYDRO POLE ON EAST SIDE OF SANFORD FLEMING DRIVE AT SOUTH WEST 2nd SUBMISSION SEPT/18 RS ISSUED FOR SITE PLAN AUG/18 RS REVISIONS DATE INITIAL

APPROVED

Drawing Name: 118076—DE01.dwg, Plotted: Oct 01, 2018